

### CHEMICAL KINETIC MECHANISM FOR COMBUSTION IN SUPERCRITICAL CARBON DIOXIDE



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**Presentation Layout:** 

> Introduction the Allam cycle and high-pressure oxyfuel combustion.

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- > Description of the modelling procedure used in the present study.

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- > Discussion of the modelling work and identification of important reactions.
- > Description of the final mechanism created and its improved performance.

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The high-pressures of the Allam-Fetvedt cycle and greater power density of  $sCO_2$  reduces the total footprint compared traditional power plants.

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Over the last 5 years, more ignition delay time data has been published allowing the validation of chemical kinetic mechanisms at these conditions.

In this study, we model ignition delay time data using four existing mechanisms and use the results to produce a new mechanism designed for high-pressure,  $sCO_2$  combustion.

The ignition delay time is an important combustion parameter which can be experimentally determined using shock tubes or rapid compression machines.

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These ignition delay times were modelled on Chemkin Pro using four chemical kinetic mechanisms which were compared using quantitative analysis using the following equation from Liu et al. (2019).

$$E = \frac{1}{N} \sum_{i=1}^{N} \left| \frac{X_{sim,i} - X_{exp,i}}{X_{exp,i}} \right| \times 100$$

Y. Liu, J. Cheng, C. Zou, L.X. Lu, H.X. Jing, Ignition delay times of ethane under O<sub>2</sub>/CO<sub>2</sub> atmosphere at different pressures by shock tube and simulation methods, Combustion and Flame 204 (2019) 380-390.

A series of sensitivity analyses were performed at temperatures where the agreement between different mechanisms was poor, of the agreement between a mechanism and the experimental data.

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Comparison of the sensitivity analysis of H3 for Aramco 2.0 and USC II at 1274 K.



S3 dataset sensitivity analysis of GRI 3.0 and Aramco 2.0 at 1280 K.



#### Methane datasets studied.

Dataset	Reference	Average Pressure	Equivalence Ratio	$CO_2$ Dilution (%)
		/atm	(Ф)	
M1	Pryor et al. (2017)	29.6	1.00	85.00
M2	Barak et al. (2020)	79.9	1.00	36.50
M3	Karimi et al. (2019)	99.0	1.00	85.00
M4	Karimi et al. (2019)	97.0	0.50	80.00
M5	Karimi et al. (2019)	201.8	1.00	85.00
M6	Shao et al. (2019)	32.2	1.00	77.50
M7	Shao et al. (2019)	106.3	1.00	77.50
M8	Shao et al. (2019)	260.0	1.00	77.50
M9	Shao et al. (2019)	31.4	1.27	86.17
M10	Shao et al. (2019)	74.7	1.27	86.17
M11	Shao et al. (2019)	266.3	1.27	86.17

O. Pryor, B. Koroglu, S. Barak, J. Lopez, E. Ninnemann, L. Nash, S. Vasu, Ignition delay times of high pressure oxy-methane combustion with high levels of CO<sub>2</sub> dilution, Proceedings of ASME Turbo Expo 2017: Turbo-machinery Technical Conference and Exposition, Charlotte, NC, USA, 2017.

S. Barak, O. Pryor, E. Ninnemann, S. Neupane, S. Vasu, X. Lu, B. Forrest, Ignition delay times of oxy-syngas and oxy-methane in supercritical CO<sub>2</sub> mixtures for direct-fired cycles, Journal of Engineering for Gas Turbines and Power 142 (2020).

M. Karimi, B. Ochs, Z.F. Liu, D. Ranjan, W.T. Sun, Measurement of methane autoignition delays in carbon dioxide and argon diluents at high pressure conditions, Combustion and Flame 204 (2019) 304-319. J.K. Shao, R. Choudhary, D.E. Davidson, R.K. Hanson, S. Barak, S. Vasu, Ignition delay times of methane and hydrogen highly diluted in carbon dioxide at high pressures up to 300 atm, Proceedings of the Combustion Institute 37 (2019) 4555-4562.



	Aramco 2.0	DTU	GRI 3.0	USC II
<b>M</b> 1	41.47	37.98	76.11	17.04
M2	17.10	12.60	54.37	9.55
M3	24.85	27.18	54.76	20.49
M4	14.26	13.44	56.66	8.24
M5	9.53	7.35	32.49	45.53
M6	60.09	47.06	23.63	38.39
M7	15.02	16.64	43.26	20.65
M8	26.87	37.65	204.32	323.56
M9	94.06	99.87	31.97	56.38
<b>M</b> 10	18.91	25.79	57.11	13.79
<b>M</b> 11	3.99	24.03	32.53	125.37
Average	29.65	31.78	60.66	61.73
No. Best Fit	3	1	2	5

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OH sensitivity coefficient against time for condition M11; a) Aramco 2.0 and b) USC II.

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-HO2 + HO2 = O2 + H2O2



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Adding the  $CH_3O_2$  Chemistry from Aramco 2.0 into the USC II mechanism significantly reduces the model's ignition delay times at these temperatures.

R5 -  $H_2O_2$  (+M) = OH +OH (+M)

 $R6 - CH_3 + HO_2 = CH_4 + O_2$ 

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Sequential changes to USC II; a) M8 and b) M11; [USC II +  $CH_3O_2$ ]: addition of  $CH_3O_2$  chemistry from Aramco 2.0, [USC II-Altered R6 +  $CH_3O_2$ ] change R6 to Aramco 2.0 rate coefficient, [USC II-Altered R5 and R6 +  $CH_3O_2$ ]: change R5 to the Aramco 2.0 rate coefficient.

#### Hydrogen datasets studied.

Dataset	Reference	Average Pressure	Equivalence	$O_2$ Dilution (%)
		/atm	Ratio ( $\Phi$ )	
H1	Shao et al. (2019)	109.6	1.00	85.00
H2	Shao et al. (2019)	270.6	1.00	85.00
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	Aramco 2.0	DTU	GRI 3.0	USC II
H1	11.43	25.12	63.45	50.70
H2	12.20	20.58	79.90	74.33
H3	89.13	116.67	112.95	70.82
Average	37.59	54.12	85.43	65.28
No. Best Fit	2	0	0	1

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 $R7 - H_2O_2 + H = H_2 + HO_2$ 

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No. Best Fit	2	0	0	1



 $R7 - H_2O_2 + H = H_2 + HO_2$ 

R8 -  $O_2$  + H = O + OH

R9 - H +  $O_2$  (+M) = H $O_2$  (+M)

Comparison of the sensitivity analysis of H3 for Aramco 2.0 and USC II at 1274 K.



H1 and H2 dataset modelled by Aramco 2.0, USC II, and [USC II-Altered R7]: USC II with the updated R7 rate coefficient

J.K. Shao, R. Choudhary, D.E. Davidson, R.K. Hanson, S. Barak, S. Vasu, Ignition delay times of methane and hydrogen highly diluted in carbon dioxide at high pressures up to 300 atm, Proceedings of the Combustion Institute 37 (2019) 4555-4562.

 $R7 - H_2O_2 + H = H_2 + HO_2$ 

Changing the rate coefficient of R7 in USC II from that of Aramco 2.0 reduces the ignition delay time and better matches the experimental data.

#### Syngas datasets studied.

Dataset	Reference	Average Pressure	Equivalence	$O_2$ Dilution (%)
		/atm	Ratio ( $\Phi$ )	
S1	Barak et al. (2020)	78.9	1.02	91.80
S2	Barak et al. (2020)	91.7	0.41	64.50
S3	Barak et al. (2020)	89.6	0.41	92.20
S4	Barak et al. (2020)	89.7	1.09	63.90
S5	Barak et al. (2018)	41.5	1.00	85.00
S6	Barak et al. (2018)	38.6	1.00	85.00
S7	Barak et al. (2018)	38.5	1.00	85.00
S8	Barak et al. (2018)	38.4	1.00	85.00

S. Barak, O. Pryor, E. Ninnemann, S. Neupane, S. Vasu, X. Lu, B. Forrest, Ignition delay times of oxy-syngas and oxy-methane in supercritical CO<sub>2</sub> mixtures for direct-fired cycles, Journal of Engineering for Gas Turbines and Power 142 (2020). S. Barak, E. Ninnemann, S. Neupane, F. Barnes, J. Kapat, S. Vasu, High-pressure oxy-syngas ignition delay times with CO<sub>2</sub> dilution: Shock tube measurements and comparison of the performance of kinetic mechanisms, Journal of Engineering for Gas Turbines and Power 141 (2018).

#### Quantitative analysis of syngas datasets

	Aramco 2.0	DTU	GRI 3.0	USC II
S1	53.20	70.06	21.84	49.96
S2	66.05	94.50	31.40	109.03
S3	117.50	181.42	32.33	123.44
S4	126.76	158.27	84.69	196.60
S5	240.64	303.37	170.24	242.84
S6	259.59	341.14	169.83	277.12
S7	191.64	277.53	241.41	132.09
S8	174.54	287.50	139.00	89.63
Average E	153.74	214.22	111.34	152.59
No. Best Fit	0	0	6	2



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Sensitivity analysis and identification of important syngas reactions.

 $R10 - CO + HO_2 = CO_2 + OH$ 



S3 dataset sensitivity analysis of GRI 3.0 and Aramco 2.0 at 1280 K.

Sensitivity analysis and identification of important syngas reactions.

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Mechanism comparison for the S3 condition with the R10 rate coefficient from Baulch et al. (1976) denoted by \*.

The challenge is to culminate the information gained from the sensitivity analysis to create one mechanism which can best model the conditions relevant to  $sCO_2$  combustion.

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USC II was chosen as a starting mechanism which was updated with rate coefficients which were identified as important through the sensitivity analysis.

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USC II was chosen as a starting mechanism which was updated with rate coefficients which were identified as important through the sensitivity analysis.

In total 16 reactions were added to incorporate important chemistry of  $CH_3O_2$  which was identified as an important intermediate in high-pressure methane combustion.

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In total 16 reactions were added to incorporate important chemistry of  $CH_3O_2$  which was identified as an important intermediate in high-pressure methane combustion.

9 reactions were altered to rate coefficients from Aramco 2.0 and GRI 3.0 to better model individual datasets.

$$E = \frac{1}{N} \sum_{i=1}^{N} \left| \frac{X_{sim,i} - X_{exp,i}}{X_{exp,i}} \right| \times 100$$

Fuel		Aramco 2.0	DTU	GRI 3.0	USC II	UoS sCO <sub>2</sub>
Hydrogen	E (%)	37.6	54.1	85.4	65.3	17.5
	No.	1	0	0	0	2
	Best Fit					
Methane	E (%)	29.7	31.8	60.7	61.7	25.1
	No.	2	0	2	4	3
	Best Fit					
Syngas	E (%)	153.7	214.2	111.3	152.6	76.2
	No.	0	0	3	0	5
	Best Fit					
Averag	e E	73.7	100.0	85.8	93.2	39.6
Total No. B	est Fit	3	0	5	4	10

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	No.	0	0	3	0	5
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	Best Fit					
Average	e E	73.7	100.0	85.8	93.2	39.6
Total No. B	est Fit	3	0	5	4	10

$$E = \frac{1}{N} \sum_{i=1}^{N} \left| \frac{X_{sim,i} - X_{exp,i}}{X_{exp,i}} \right| \times 100$$

Fuel		Aramco 2.0	DTU	GRI 3.0	USC II	UoS sCO <sub>2</sub>
Hydrogen	E (%)	37.6	54.1	85.4	65.3	17.5
	No.	1	0	0	0	2
	Best Fit					
Methane	E (%)	29.7	31.8	60.7	61.7	25.1
	No.	2	0	2	4	3
	Best Fit					
Syngas	E (%)	153.7	214.2	111.3	152.6	76.2
	No.	0	0	3	0	5
	Best Fit					
Average	e E	73.7	100.0	85.8	93.2	39.6
Total No. B	est Fit	3	0	5	4	10

# Chemical Kinetic Mechanism for Combustion in Supercritical Carbon Dioxide

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# Thank you for listening, any questions?

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