

PEREGRINE TURBINE TECHNOLOGIES

# Experimental Testing of a 1MW sCO2 Turbocompressor





Logan Rapp Sandia National Laboratories 3<sup>rd</sup> European sCO2 Conference September 20, 2019

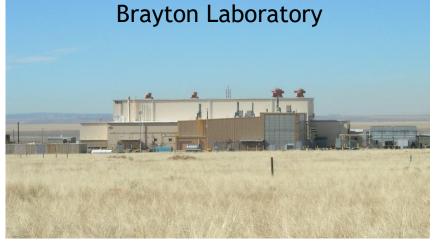
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SAND2019-10928 C



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#### <sup>2</sup> History of sCO2 research at Sandia National Laboratories





Turbomachinery Testing



Heat Exchanger Testing



**Bearings Testing** 



#### Pressure Fatigue Testing



Seals Testing

## Recompression Closed Brayton Cycle (RCBC) configuration

#### Commissioned in 2012

Only experimental sCO2 RCBC ever to have been operated

Many papers and conference proceedings have been published on the data from the RCBC experiments



## 4 TurboMachinery Development Platform at SNL

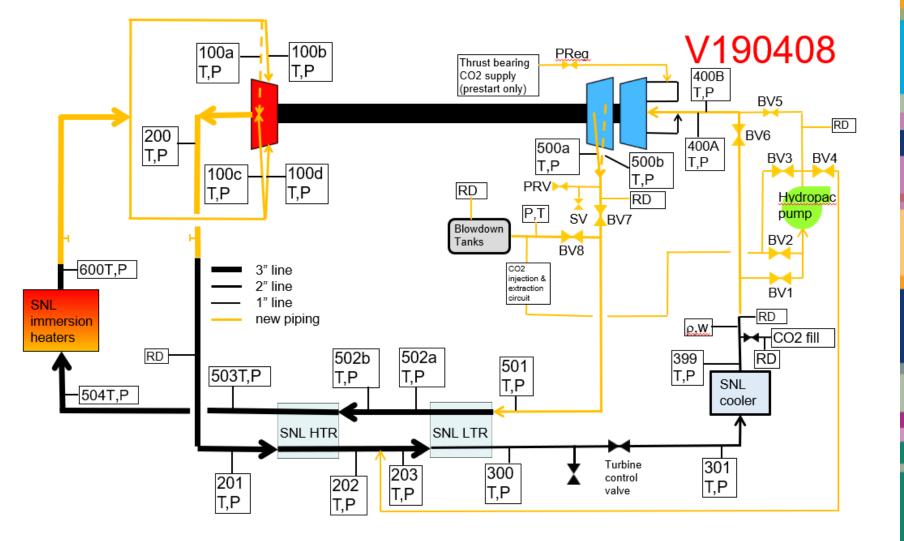
780 kW electric immersion heat

2.3 MW duty High Temp Recuperator

1.6 MW duty Low Temp Recuperator

540 kW water/sCO2 cooler

Hydro-Pac Piston compressor pump

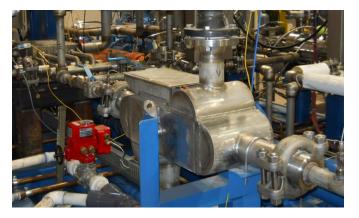


## 5 TurboMachinery Development Platform at SNL









## <sup>6</sup> Peregrine Turbine Technologies Turbocompressor

Design Conditions:

- 118,000 RPM
- 750 C Turbine Inlet (1382 F)
- 42.9 MPa compressor discharge (6222 psi)

Loop Maximum Conditions:

- 538 C Turbine Inlet (1000 F)
- 17.2 MPa compressor discharge (2500 psi)



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#### 7 Blowdown Start Method

Loop is preconditioned using Hydropac

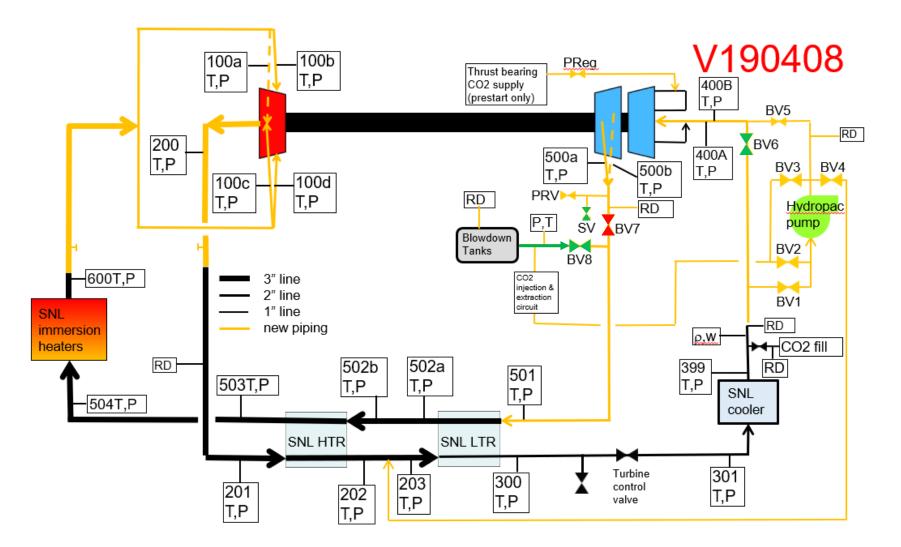
- Compressor inlet above supercritical conditions
- Turbine inlet at approximately target for test

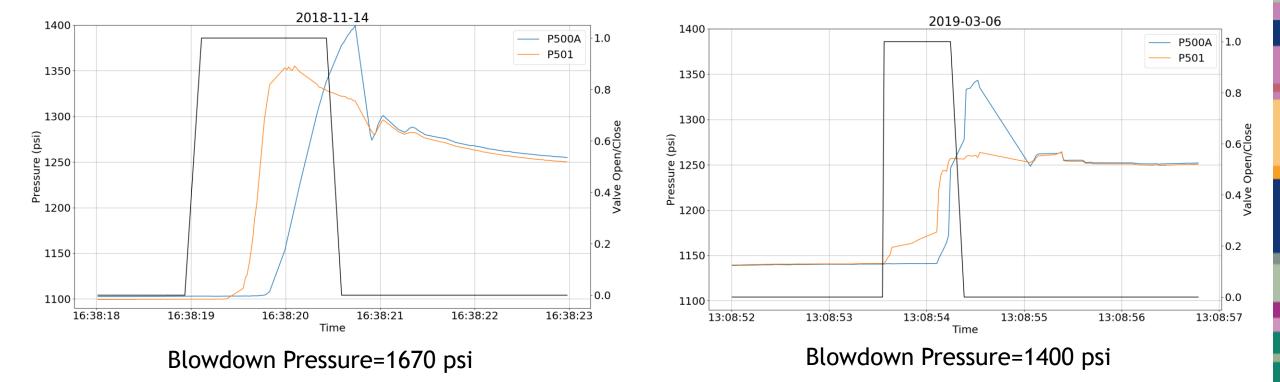
Valve Positions

- BV7 is closed
- BV8 and SV are opened

Once P500A - P501 > dP\_min:

 BV7 is opened and BV8 and SV are closed





8 Blowdown start plots

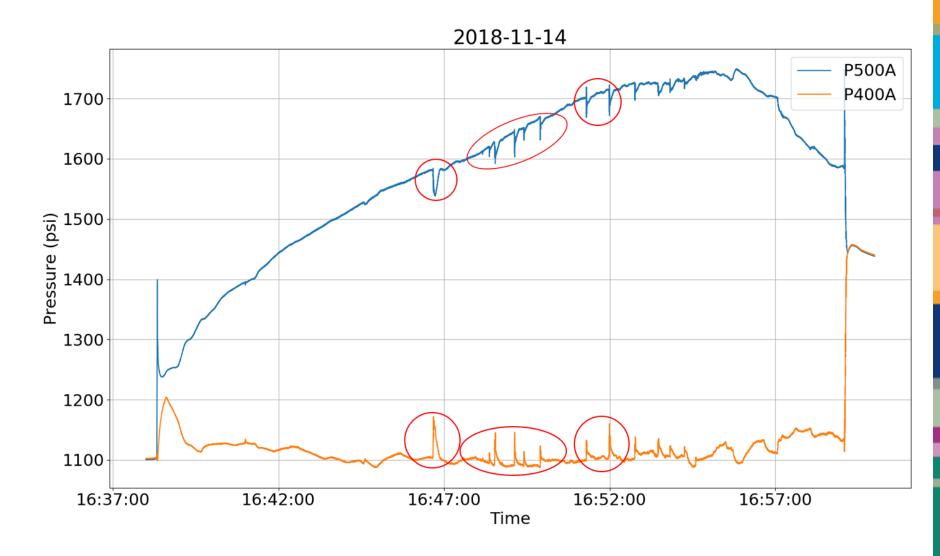
# 9 Summary of tests to date

Test Number	Test Date	Test Duration	TIT (°F)	Compressor Discharge Pressure (psi)	Max PR
1	8/9/2018	00:00:32	225	1240	1.2
2	10/10/2018	00:18:40	420	1400	1.25
3	11/14/2018	00:20:46	645	1750	1.59
4	3/1/2019	00:03:32	610	1460	1.26
5	3/6/2019	00:08:23	530	1510	1.3
6	4/4/2019	00:03:18	530	1510	1.28
7	5/7/2019	8:05:44	570	1475	1.27

#### 10 Bearing Issues

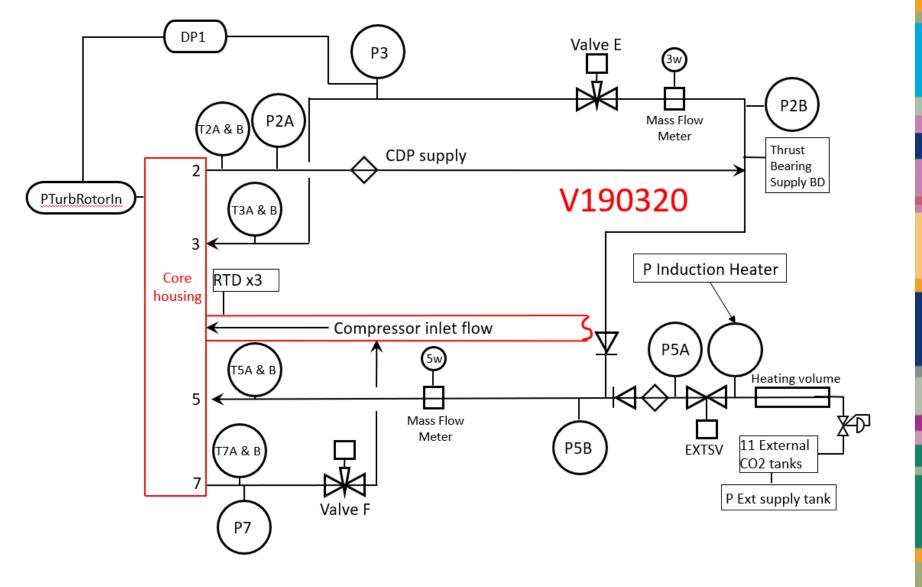
In Tests #1-3, both the thrust bearing and the radial bearings experienced rubs/failures

Spikes in pressure indicate thrust bearing rubs

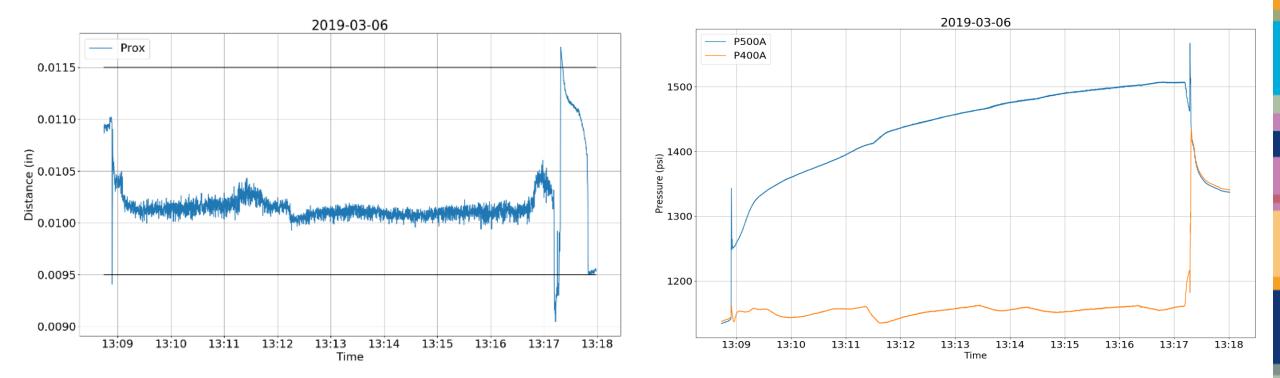


#### 11 Secondary Flows

Valve F regulates venting pressure on aft side of thrust disk rotor – acts as balance piston



#### 12 Thrust bearing issue resolved



By adjusting Valve F and the TCV the force on the rotor was balanced.

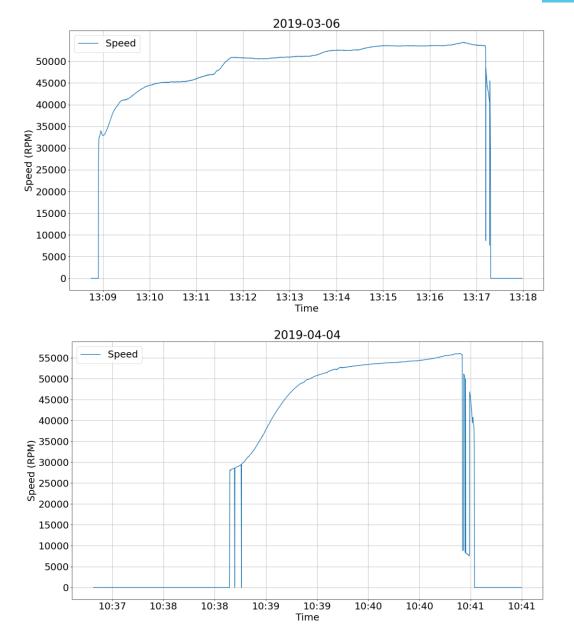
#### 

#### 13 Radial Bearing Issues

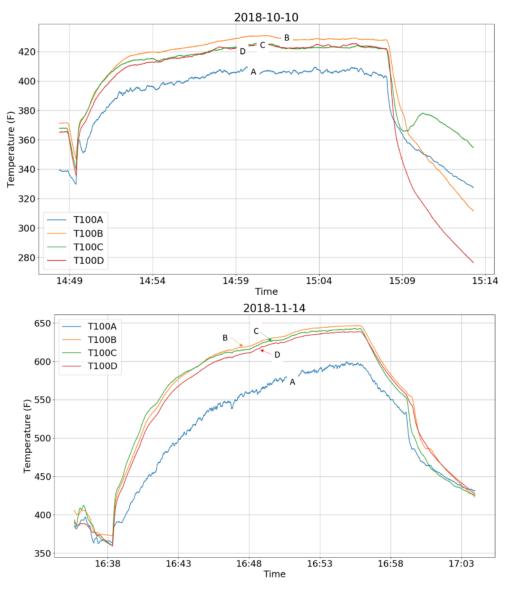
In all tests (except #7 - 8 hr test), the turbine end radial bearing failed

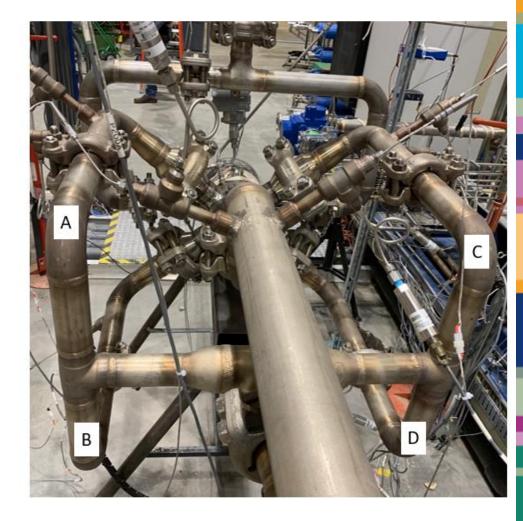
Possible causes of failure:

- Blowdown start
  - Reduce blowdown pressure
- Critical speed causing rotor instability
  - Physical evidence of bearing failure shows yielded foils at a specific clocking; not indication of rotor instability
- Radial load caused by non-uniform turbine inlet conditions
  - Resolved with instrumentation



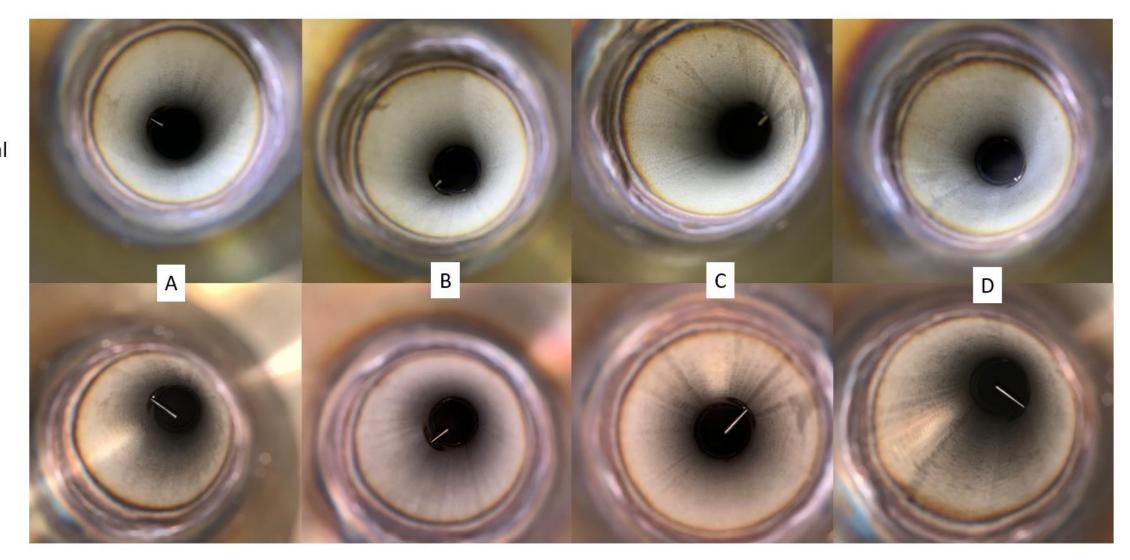
#### 14 **Turbine Inlets**





Leg "A" was consistently lower temperature than the other 3

## <sup>15</sup> Original and New Turbine Inlet RTD insertions

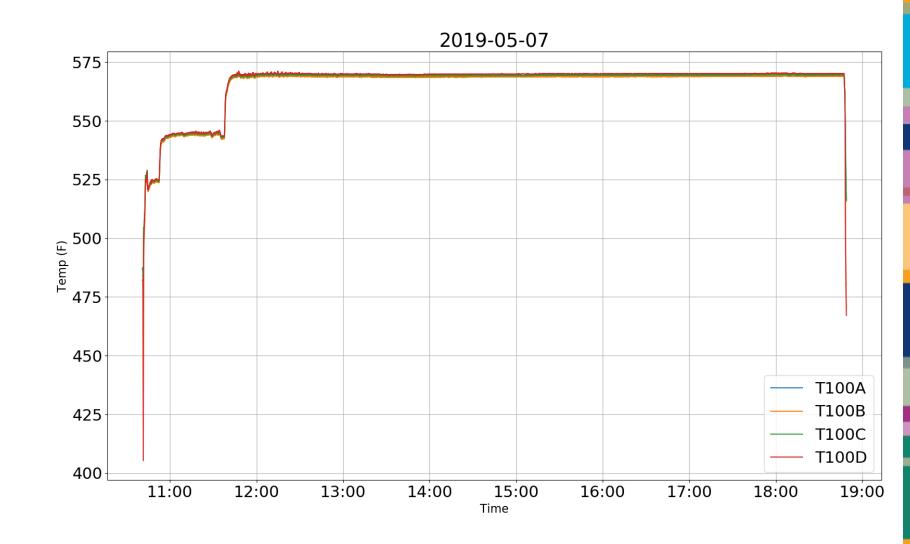


Original

New

#### <sup>16</sup> **Turbine Inlet Temp with new Insertion depth**

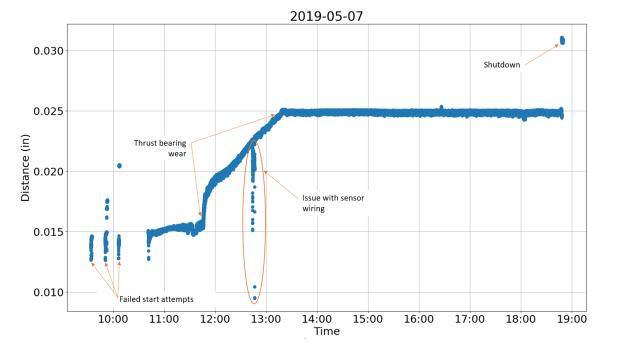
No difference in centerline temperature of turbine inlets

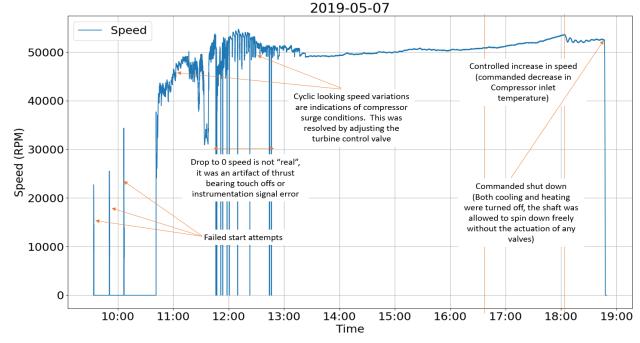


#### <sup>17</sup> Increased L/D of aft radial bearing

The aft radial bearing length/diameter ratio was increased to increase load capacity and the damping of the bearing

Start Number	Turbine Inlet Temp (F)	Blowdown Pressure (psi)	Outcome
1	460	1330	Unsuccessful
2	500	1360	Unsuccessful
3	525	1425	Unsuccessful
4	550	1450	Successful





#### 18 Next Steps

Test turbocompressor up to limits of current loop (1000F @ 2500 psi) Run sensitivity tests of turbocompressor performance with compressor inlet temperature Map performance of turbocompressor over variety of off-design conditions Work with Peregrine Turbine Technologies to test turbocompressor up to full design conditions

# Thank you