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Accurate and Predictive Mixture Models Applied to Mixtures with CO₂

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Outline

Introduction and Motivation

Multi-Fluid Mixture Models

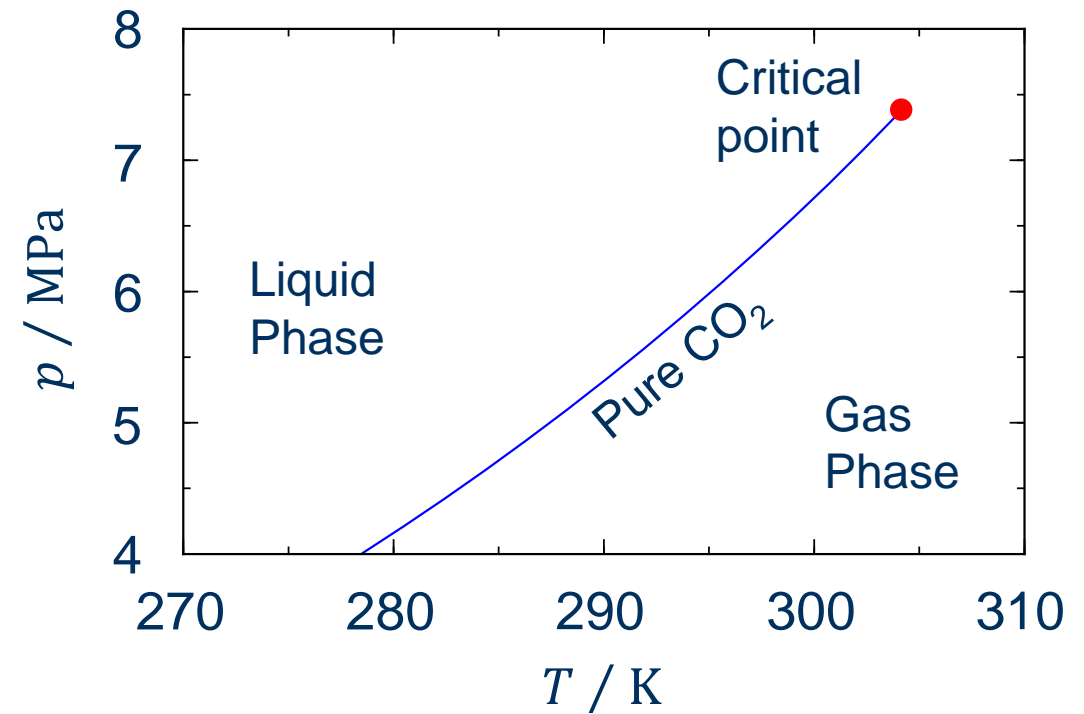
Results for Phase Equilibria

Results for Homogeneous Densities

Summary and Perspective

Introduction and Motivation

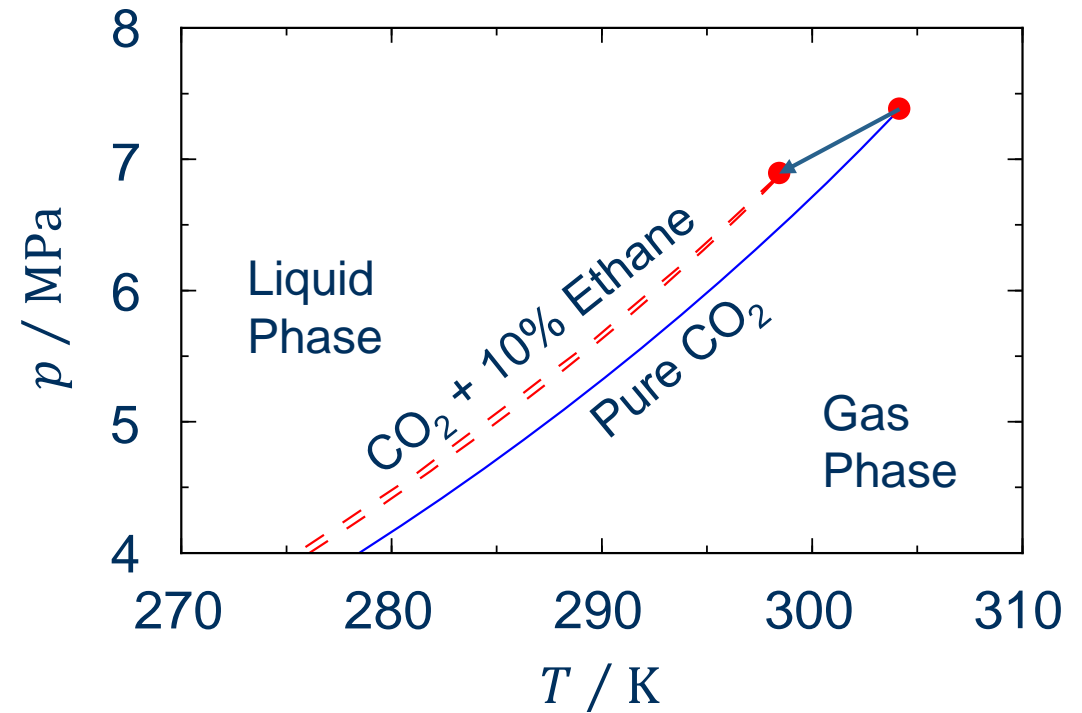
- The efficiency of processes with sCO₂ can be potentially optimized by using blends
- Example: Shift of critical point



Introduction and Motivation

- The efficiency of processes with sCO₂ can be potentially optimized by using blends
- Example: Shift of critical point

→ Models needed to find promising mixtures



Introduction and Motivation

- Multiparameter equations of state (e.g. Span and Wagner (1996)) can be used in a multi-fluid mixture model (Lemmon and Tillner-Roth (1999), Kunz and Wagner (2012))
- For accurate models, usually many parameters need to be fitted to experimental data
- Standard mixing rules for predictive calculations do not always give good results
- Recently, we proposed a predictive model, which yields good results for phase equilibria
- Representation of homogeneous properties is studied in this work
- Here: CO_2+CH_4 and $\text{CO}_2+\text{C}_2\text{H}_6$ studied

Multi-Fluid Mixture Models

The multi-fluid mixture model can be written as follows

$$\frac{a}{RT} = \alpha(\tau, \delta, \bar{x}) = \sum_{i=1}^N x_i \underbrace{\alpha_{0,i}^o(T, \rho)}_{\text{Pure substance}} + \underbrace{\sum_{i=1}^N x_i \ln(x_i)}_{\text{Ideal mixing}}$$

Mixture of ideal gases:

No adjustable parameters

$$\sum_{i=1}^N x_i \underbrace{\alpha_{0,i}^r(\tau, \delta)}_{\text{Pure substance}} + \underbrace{\sum_{i=1}^{N-1} \sum_{j=i+1}^N x_i x_j F_{ij} \alpha_{ij}^r(\tau, \delta)}_{\text{Departure function}}$$

Residual part:

Arbitrary number of adjustable parameters

$$\alpha_{ij}^r = \sum_{k=1}^{K_{\text{Pol},ij}} n_{ij,k} \delta^{d_{ij,k}} \tau^{t_{ij,k}} + \alpha_{ij,\text{EXP}}^r + \dots$$

Multi-Fluid Mixture Models

The multi-fluid mixture model can be written as follows

$$\frac{a}{RT} = \alpha(\tau, \delta, \bar{x}) = \sum_{i=1}^N x_i \underbrace{\alpha_{0,i}^o(T, \rho)}_{\text{Pure substance}} + \underbrace{\sum_{i=1}^N x_i \ln(x_i)}_{\text{Ideal mixing}}$$

$$\sum_{i=1}^N x_i \underbrace{\alpha_{0,i}^r(\tau, \delta)}_{\text{Pure substance}} + \underbrace{\sum_{i=1}^{N-1} \sum_{j=i+1}^N x_i x_j F_{ij} \alpha_{ij}^r(\tau, \delta)}_{\text{Departure function}}$$

$$\alpha_{ij}^r = \sum_{k=1}^{K_{\text{Pol},ij}} n_{ij,k} \delta^{d_{ij,k}} \tau^{t_{ij,k}} + \alpha_{ij,\text{EXP}}^r + \dots$$

REF-MOD

Kunz and Wagner (2012)

Multi-Fluid Mixture Models

The reducing parameters are a function of the composition

$$\tau = \frac{T_{\text{red}}(\bar{x})}{T} \quad T_{\text{red}} = \sum_{i=1}^N \sum_{j=1}^N x_i x_j \beta_{T,ij} \gamma_{T,ij} \frac{(x_i + x_j)}{\beta_{T,ij}^2 x_i + x_j} (T_{c,i} T_{c,j})^{0.5}$$
$$\delta = \frac{\rho}{\rho_{\text{red}}(\bar{x})} \quad \frac{1}{\rho_{\text{red}}} = v_{\text{red}} = \sum_{i=1}^N \sum_{j=1}^N x_i x_j \beta_{v,ij} \gamma_{v,ij} \frac{(x_i + x_j)}{\beta_{v,ij}^2 x_i + x_j} \frac{1}{8} \left(\frac{1}{\rho_{c,i}^{1/3}} + \frac{1}{\rho_{c,j}^{1/3}} \right)^3$$

Multi-Fluid Mixture Models

If no experimental data are available

→ **Standard mixing rules** for reducing parameters

Linear mixing rules

$$\beta_T = 1 ; \beta_v = 1 ; \gamma_T = \frac{1}{2} \frac{(T_{c,i} + T_{c,j})}{(T_{c,i} \cdot T_{c,j})^{0,5}} ; \gamma_v = 4 \frac{(v_{c,i} + v_{c,j})}{(v_{c,i}^{1/3} + v_{c,j}^{1/3})^3}$$

$$\rightarrow T_{\text{red}} = \sum_{i=1}^N x_i T_{c,i} \quad \text{and} \quad v_{\text{red}} = \sum_{i=1}^N x_i v_{c,i}$$

No departure function $\alpha_{ij}^r = 0$

LIN-MOD

Multi-Fluid Mixture Models

The multi-fluid mixture model can be written as follows

$$\frac{a}{RT} = \alpha(\tau, \delta, \bar{x}) = \sum_{i=1}^N x_i \underbrace{\alpha_{o,i}^o(T, \rho)}_{\text{Pure substance}} + \underbrace{\sum_{i=1}^N x_i \ln(x_i)}_{\text{Ideal mixing}} +$$
$$\sum_{i=1}^N x_i \underbrace{\alpha_{o,i}^r(\tau, \delta)}_{\text{Pure substance}} + \underbrace{\alpha^{\text{DEP}}}_{\text{Departure function}}$$

Combination of Multi-Fluid Mixture Models with g^E -Models

The theoretically based departure function reads (Jäger et al. (2018a, 2018b))

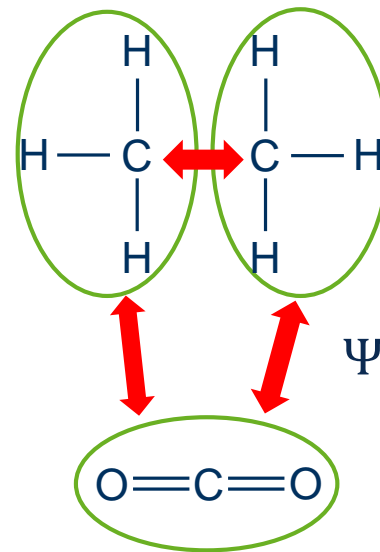
$$\alpha^{\text{Dep}} = \frac{\ln(1 + b\rho)}{\ln(1 + b\rho_{\text{ref}})} \left\{ \frac{g_{\text{GE}}^{\text{E,r}}}{RT} - \sum_{i=1}^N x_i [\alpha_{oi}^{\text{r}}(\delta_{\text{ref}}, \tau) - \alpha_{oi}^{\text{r}}(\delta_{i,\text{ref}}, \tau_i)] \right\}$$

UNIFAC

Fredenslund et al. (1975)

Parameters of the VTPR (Schmid and Gmehling (2012), Schmid et al. (2014))

$$g^{\text{E,r}} = RT \sum_{i=1}^N x_i \ln(\gamma_i^{\text{r}})$$



$$\Psi_{nm} = \exp\left(-\frac{a_{nm} + b_{nm}T + c_{nm}T^2}{T}\right)$$

UNI-MOD

Combination of Multi-Fluid Mixture Models with g^E -Models

The theoretically based departure function reads (Jäger et al. (2018a, 2018b))

$$\alpha^{\text{Dep}} = \frac{\ln(1 + b\rho)}{\ln(1 + b\rho_{\text{ref}})} \left\{ \frac{g_{\text{GE}}^{\text{E,r}}}{RT} - \sum_{i=1}^N x_i [\alpha_{oi}^r(\delta_{\text{ref}}, \tau) - \alpha_{oi}^r(\delta_{i,\text{ref}}, \tau_i)] \right\}$$

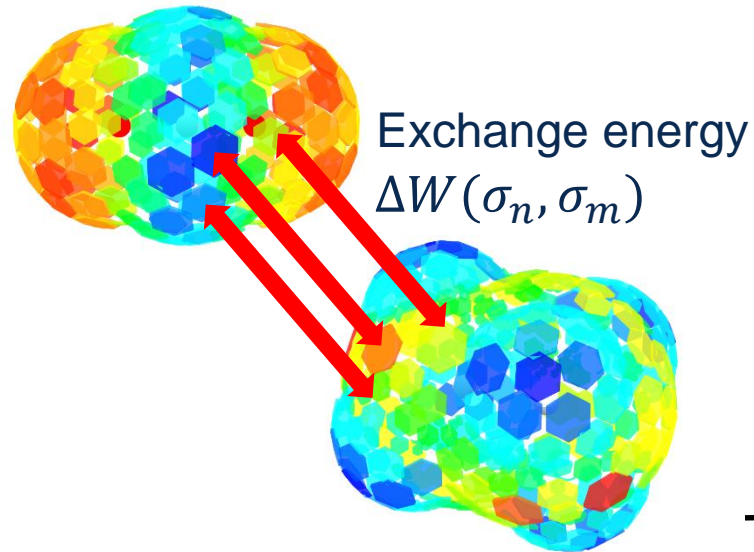
COSMO-SAC

Lin and Sandler (2002) (COSMO-SAC 1)

Hsieh et al. (2010) (COSMO-SAC 2)

Hsieh et al. (2014) (COSMO-SAC 3)

$$g^{\text{E,r}} = RT \sum_{i=1}^N x_i \ln(\gamma_i^{\text{r}})$$



COS1-MOD

COS2-MOD

COS3-MOD

Thermophysical Property Software (TREND)

— All models are implemented in a user-friendly software tool (TREND 4.0)

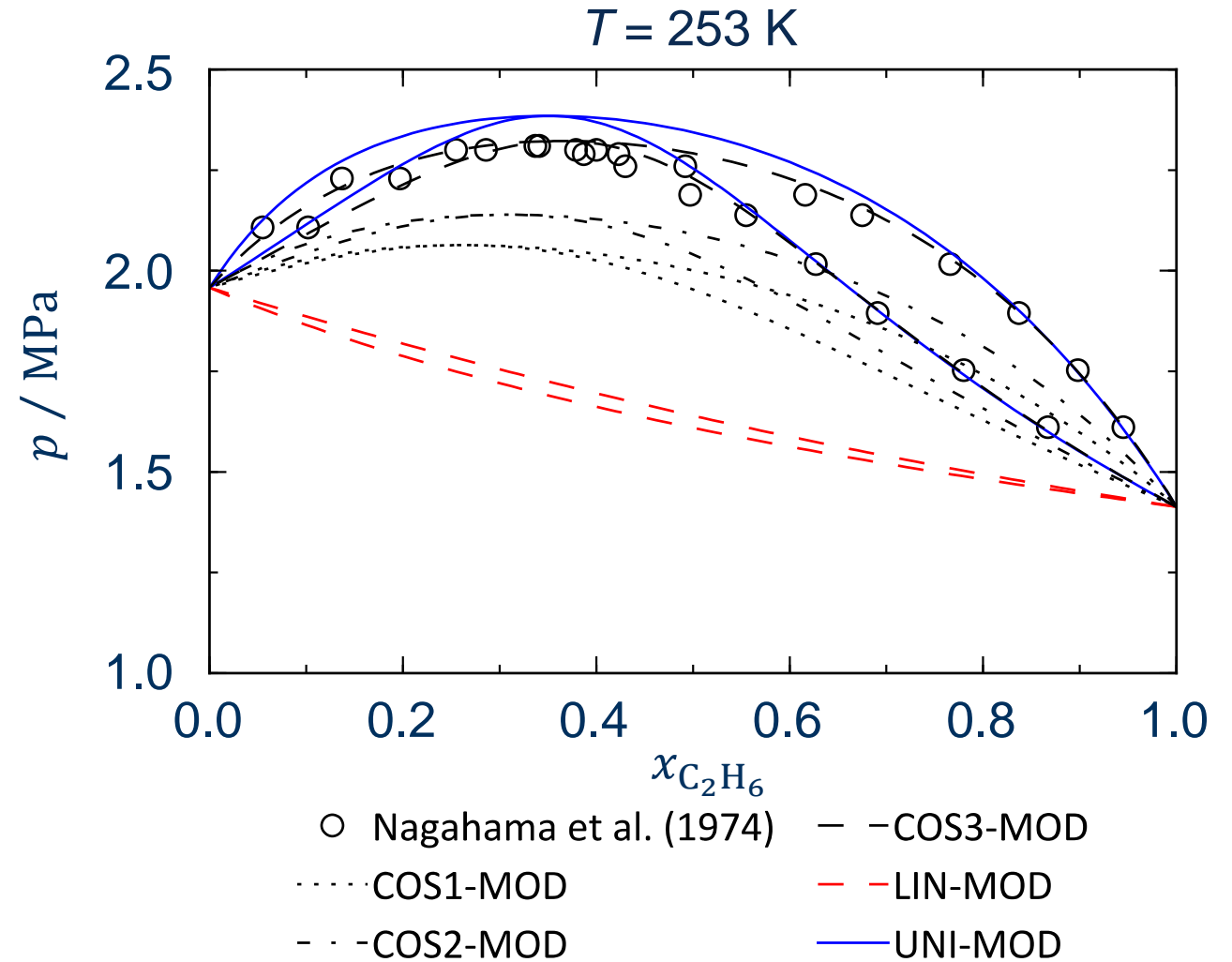
INPUT PARAMETERS				FLASH CALCULATION					
Path to EOS	D:\Arbeit\Stoffdatensoftwares\TREND_d			vap	liq1	liq2	sol	hyd	Overall
Input code	tp			temperature	K	253,000		253,000	253,000
Property 1	253 K			pressure	MPa	1,850		1,850	1,850
Property 2	1,85 MPa			density	mol/m ³	1156,908		15243,80	4819,935
Unit	molar			int. energy	j/mol	15520,343		6268,134807	7911,433
				enthalpy	j/mol	17119,433		6389,496	8295,256
				entropy	j/(mol K)	76,803		32,374	40,265
				gibbs energy	j/mol	-2311,644		-1801,074	-1891,757
				helmholtz energy	j/mol	-3910,735		-1922,435	-2275,580
				isob. heat capacity	j/(mol K)	68,094		95,446	-6666,000
				isoch. heat capacity	j/(mol K)	41,349		45,321	-6666,000
				speed of sound	m/s	231,397		684,036	-6666,000
				hydration number	-				
				hydrate structure	-				
				overall small cage occup	-				
				overall large cage occup	-				
				molecular weight	kg/mol	0,034		0,033	0,033
				phase fraction	mol/mol	0,177611491		0,82238851	
				x1	mol/mol	0,310125		0,176216	co2
				x2	mol/mol	0,689875		0,823783706	ethane

Results Phase Equilibria CO₂+C₂H₆

— Other models typically yield better results for phase equilibria than LIN-MOD

— COS3-MOD:
Adjusted dispersion parameter

$$\frac{\varepsilon_{\text{CO}_2}}{k_B} = 85 \text{ K}$$



Results Phase Equilibria CO₂+C₂H₆

— More results for phase equilibria can be found in our recent works

Jäger et al. (2018a)

Fluid Phase Equilibria 469 (2018) 56–69



A theoretically based departure function for multi-fluid mixture models[☆]

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Jäger et al. (2018b)

Fluid Phase Equilibria 476 (2018) 147–156



A combination of multi-fluid mixture models with COSMO-SAC

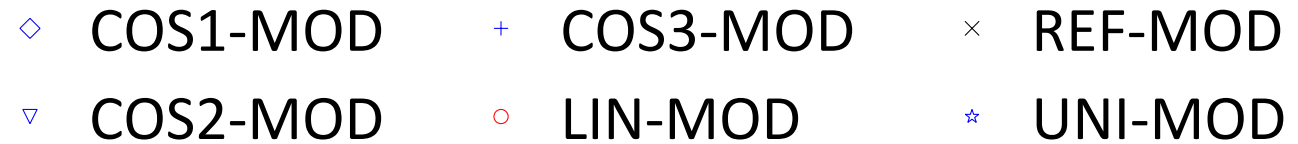
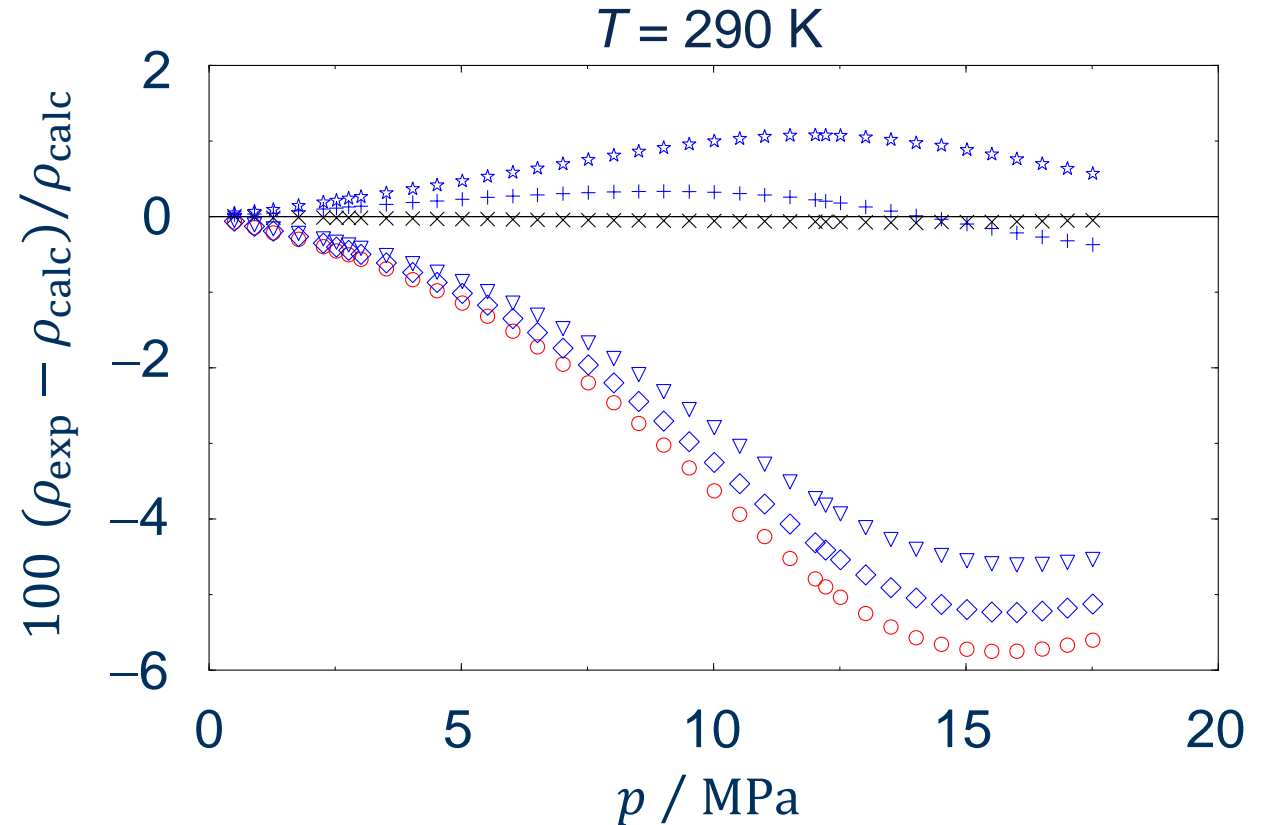
Andreas Jäger^{*}, Erik Mickoleit, Cornelia Breitung

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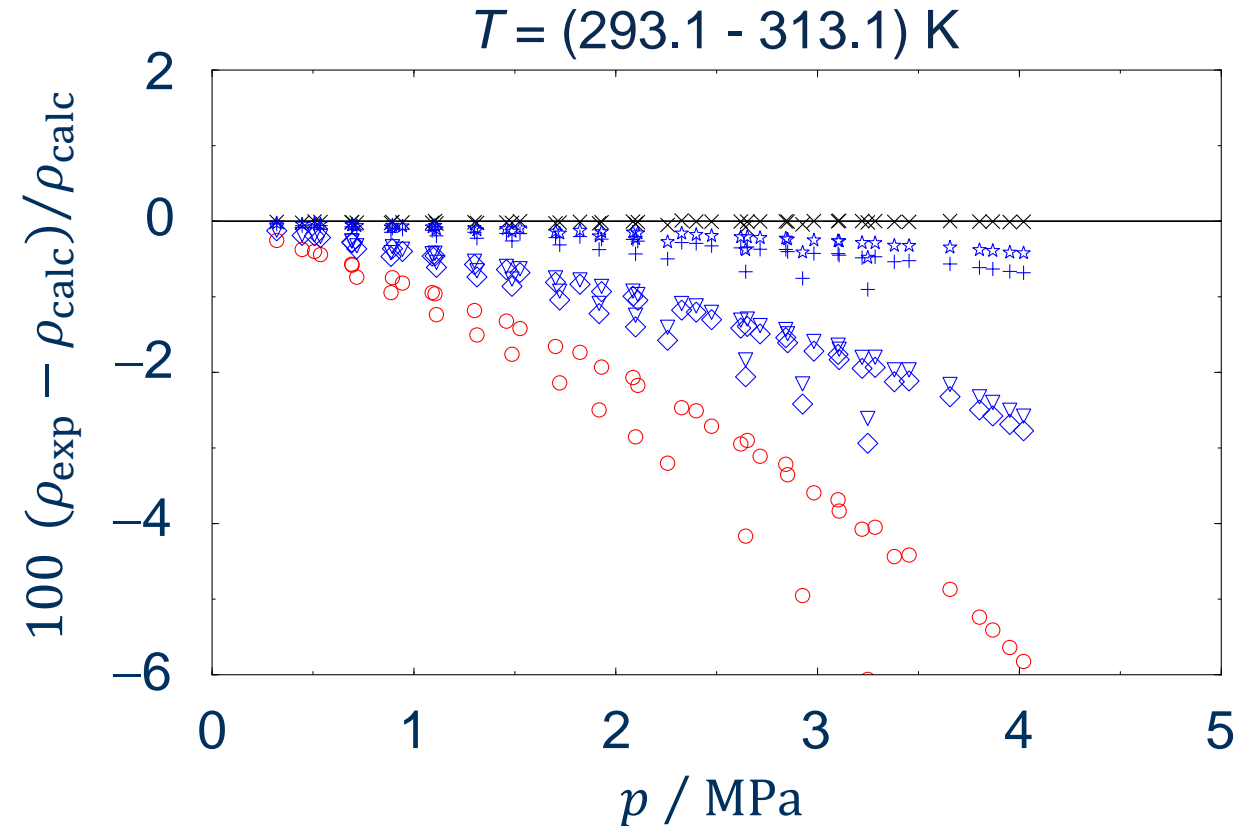
Results Homogeneous Densities CO₂+CH₄

- Experimental data by Jaeschke et al. (1991, 1997)
- Uncertainty of the data approx. 0.1%
- Tendency visible that predictive models UNI-MOD, COS1-MOD, COS2-MOD, COS3-MOD yield better results than LIN-MOD



Results Homogeneous Densities $\text{CO}_2 + \text{C}_2\text{H}_6$

— Tendency visible that predictive models UNI-MOD, COS1-MOD, COS2-MOD, COS3-MOD yield better results than LIN-MOD



◇	COS1-MOD	+	COS3-MOD	×	REF-MOD
▽	COS2-MOD	○	LIN-MOD	☆	UNI-MOD

Summary

- Predictive multi-fluid mixture models and reference models have been compared to experimental data
- Investigated mixtures: CO_2+CH_4 and $\text{CO}_2+\text{C}_2\text{H}_6$
- Results for phase equilibria are better for UNI-MOD and COS-MOD than with LIN-MOD
- Unexpectedly, homogeneous densities are also better with UNI-MOD and COS-MOD than with LIN-MOD
- Hence, the combination of the multi-fluid mixture model with g^E -models seems to be better suited for screening purposes than LIN-MOD

Perspective

- Further comparisons needed:
 - Other mixtures
 - More properties (speed of sound, heat capacity, etc.)
- The effect of refitting (general) parameters of UNIFAC and COSMO-SAC should be studied
- The developed models can be used for screenings for promising mixtures
- Further development of these models: TU Dresden, suCOO-Lab

Thank you for your attention!
Questions?

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Combination of Multi-Fluid Mixture Models with g^E -Models

Basic idea: equate g^E or a^E at a specified reference pressure

$$g_{\text{EOS}}^E(p_0) = g_{\text{GE}}^E \quad a_{\text{EOS}}^E(p_0) = a_{\text{GE}}^E$$

Needed: expression for a^E from multi-fluid mixture model

$$a^E(T, p, \bar{x}) = a(T, p, \bar{x}) - RT \sum_{i=1}^N x_i \ln(x_i) - \sum_{i=1}^N x_i a_{oi}(T, p)$$

Molar Helmholtz energy of the mixture at specified T, p, \bar{x}

Ideal mixing term

Molar Helmholtz energies of the pure components i at specified T, p

Combination of Multi-Fluid Mixture Models with g^E -Models

Molar Helmholtz energy of the **mixture** calculated with the multi-fluid mixture model

$$\frac{a(T, p, \bar{x})}{RT} = \alpha(\tau, \delta, \bar{x}) = \sum_{i=1}^N x_i \alpha_{0,i}^o(T, \rho) + \sum_{i=1}^N x_i \ln(x_i) + \sum_{i=1}^N x_i \alpha_{0,i}^r(\tau, \delta) + \alpha^{\text{Dep}}(T, p, \bar{x})$$

The Helmholtz energy of the mixture needs to be evaluated at T, p und \bar{x}

$$\rho = \rho(T, p, \bar{x}) \rightarrow \delta = \frac{\rho(T, p, \bar{x})}{\rho_{\text{red}}(\bar{x})}$$

$$\tau = \frac{T_{\text{red}}(\bar{x})}{T}$$

Combination of Multi-Fluid Mixture Models with g^E -Models

Molar Helmholtz energy of the **pure components**

$$\frac{a_{oi}(T, p)}{RT} = \alpha_{o,i}^0(T, \rho_i) + \alpha_{o,i}^r(\tau_i, \delta_i)$$

The Helmholtz energies need to be evaluated at the same T and p :

$$\rho_i = \rho_i(T, p) \rightarrow \delta_i = \frac{\rho_i(T, p)}{\rho_{c,i}}$$

$$\tau_i = \frac{T_{c,i}}{T}$$

Combination of Multi-Fluid Mixture Models with g^E -Models

The molar excess Helmholtz energy then becomes

$$\frac{a^E(T, p, \bar{x})}{RT} = \sum_{i=1}^N x_i [\alpha_{0,i}^0(T, \rho) - \alpha_{0,i}^0(T, \rho_i)] + \sum_{i=1}^N x_i [\alpha_{0,i}^r(\tau, \delta) - \alpha_{0,i}^r(\tau_i, \delta_i)] + \alpha^{\text{Dep}}(T, p, \bar{x})$$

With

$$\alpha_{0,i}^0(T, \rho) = f_i(T) + \ln\left(\frac{\rho}{\rho_{c,i}}\right) \quad \text{and} \quad \alpha_{0,i}^0(T, \rho_i) = f_i(T) + \ln\left(\frac{\rho_i}{\rho_{c,i}}\right)$$

it is

$$\frac{a^E(T, p, \bar{x})}{RT} = \sum_{i=1}^N x_i \ln\left(\frac{\rho}{\rho_i}\right) + \sum_{i=1}^N x_i [\alpha_{0,i}^r(\tau, \delta) - \alpha_{0,i}^r(\tau_i, \delta_i)] + \alpha^{\text{Dep}}(T, p, \bar{x})$$

Combination of Multi-Fluid Mixture Models with g^E -Models

Finally, the departure function becomes

$$\alpha^{\text{Dep}}(T, p, \bar{x}) = \frac{a^E(T, p, \bar{x})}{RT} - \sum_{i=1}^N x_i \ln \left(\frac{\rho}{\rho_i} \right) - \sum_{i=1}^N x_i [\alpha_{o,i}^r(\tau, \delta) - \alpha_{o,i}^r(\tau_i, \delta_i)]$$

Choice of a reference pressure:

- Like PSRK (Holderbaum and Gmehling (1991))
- Saturated liquid at $p_0 = 101325 \text{ Pa}$
- Assumption of a constant packing fraction u at saturated liquid conditions

Combination of Multi-Fluid Mixture Models with g^E -Models

The following assumptions are used:

- The reference pressure is chosen as $p_0 = 101325$ Pa (see PSRK, VTPR)
- The densities of the liquid phase at p_0 are calculated assuming (see PSRK, VTPR)

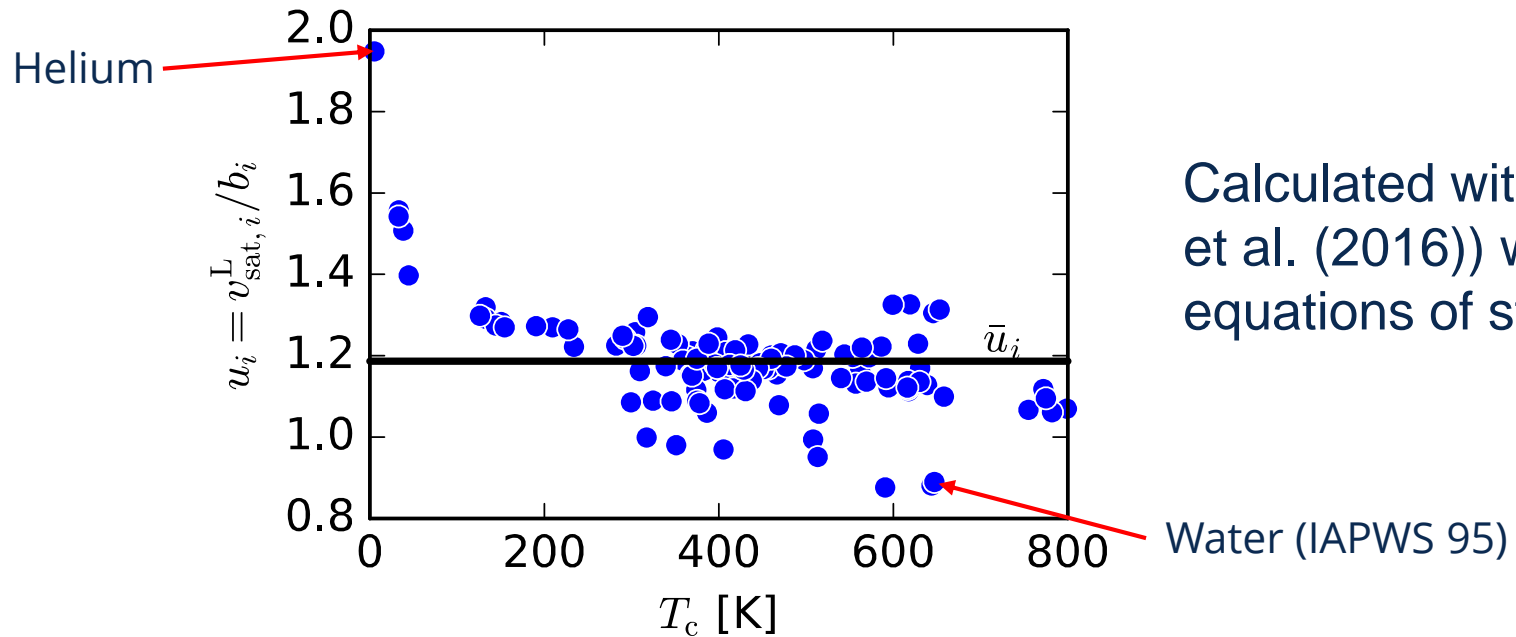
$$u = 1.17 = \text{const.} \quad \text{Inverse packing fraction:} \quad u = \frac{v_s^L(p_0)}{b} = \frac{v_{s,i}^L(p_0)}{b_i}$$

- The densities at the reference pressure then become

$$\rho_{\text{ref}} = \frac{1}{ub} \quad \text{and} \quad \rho_{i,\text{ref}} = \frac{1}{ub_i}$$

Combination of Multi-Fluid Mixture Models with g^E -Models

Calculated inverse packing fractions of saturated liquids at p_0



Calculated with TREND 3.0 (Span et al. (2016)) with multiparameter equations of state for 121 fluids

→ $\bar{u}_i \approx 1.17$ → $u = u_i = 1.17$

~~$\rho_{i,\text{ref}} = \frac{1}{u b_i}$~~ → $\rho_{i,\text{ref}} = \rho_{s,i}(p_0)$

Combination of Multi-Fluid Mixture Models with g^E -Models

The inverse packing fraction is defined as

$$u = \frac{v^L}{b}$$

u - Inverse packing fraction

v^L - Molar volume of the saturated liquid

b - covolume calculated with a cubic equation of state

For pure substances: $u_i = \frac{v_i^L}{b_i}$ with $b_i = 0.08664 \frac{RT_{c,i}}{p_{c,i}}$

The covolume of the mixture is calculated with a linear mixing rule $b = \sum_{i=1}^N x_i b_i$

Combination of Multi-Fluid Mixture Models with g^E -Models

With the definition of the inverse packing fraction follows

$$\rho_{\text{ref}} = \frac{1}{ub} \quad \text{and} \quad \rho_{i,\text{ref}} = \frac{1}{ub_i} \quad \text{Densities of saturated liquid at } p_0$$

Hence, the reduced densities at reference conditions become

$$\delta_{\text{ref}} = \frac{1}{ub\rho_r} \quad \text{and} \quad \delta_{i,\text{ref}} = \frac{1}{ub_i\rho_{c,i}}$$

And therefore the departure function

$$\alpha^{\text{Dep}} = \frac{a^E}{RT} - \sum_{i=1}^N x_i \ln \left(\frac{b_i}{b} \right) - \sum_{i=1}^N x_i [\alpha_{oi}^r(\delta_{\text{ref}}, \tau) - \alpha_{oi}^r(\delta_{i,\text{ref}}, \tau_i)]$$

Combination of Multi-Fluid Mixture Models with g^E -Models

The residual part should hold: $\lim_{\rho \rightarrow 0} \alpha^r = 0$. Therefore, a density dependent term is needed.

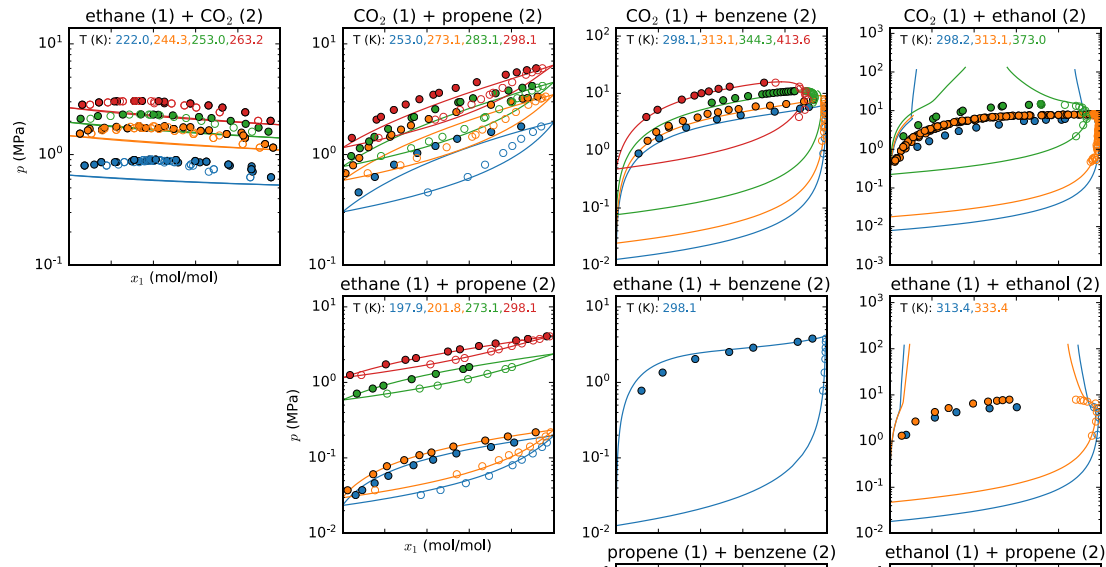
Translating the PSRK to the reduced residual Helmholtz energy, the following is obtained

$$\alpha_{\text{PSRK}}^r = -\ln(1 - b\rho) + \frac{\ln(1 + b\rho)}{\ln\left(1 + \frac{1}{u}\right)} \left\{ \frac{g_{\text{GE}}^E}{RT} - \sum_{i=1}^N x_i \ln\left(\frac{b_i}{b}\right) - \frac{1}{RT} \ln\left(1 + \frac{1}{u}\right) \sum_{i=1}^N x_i \frac{a_i}{b_i} \right\}$$

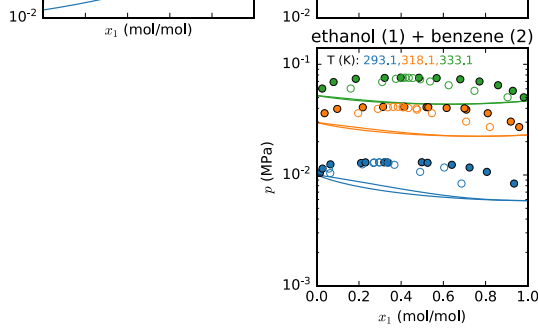
Applying the density dependent term of the PSRK yields:

$$\alpha^{\text{Dep}} = \frac{\ln(1 + b\rho)}{\ln\left(1 + \frac{1}{u}\right)} \left\{ \frac{a_{\text{GE}}^E}{RT} - \sum_{i=1}^N x_i \ln\left(\frac{b_i}{b}\right) - \sum_{i=1}^N x_i [\alpha_{oi}^r(\delta_{\text{ref}}, \tau) - \alpha_{oi}^r(\delta_{i,\text{ref}}, \tau_i)] \right\}$$

Results for All Binary Mixtures With Linear Mixing Rules

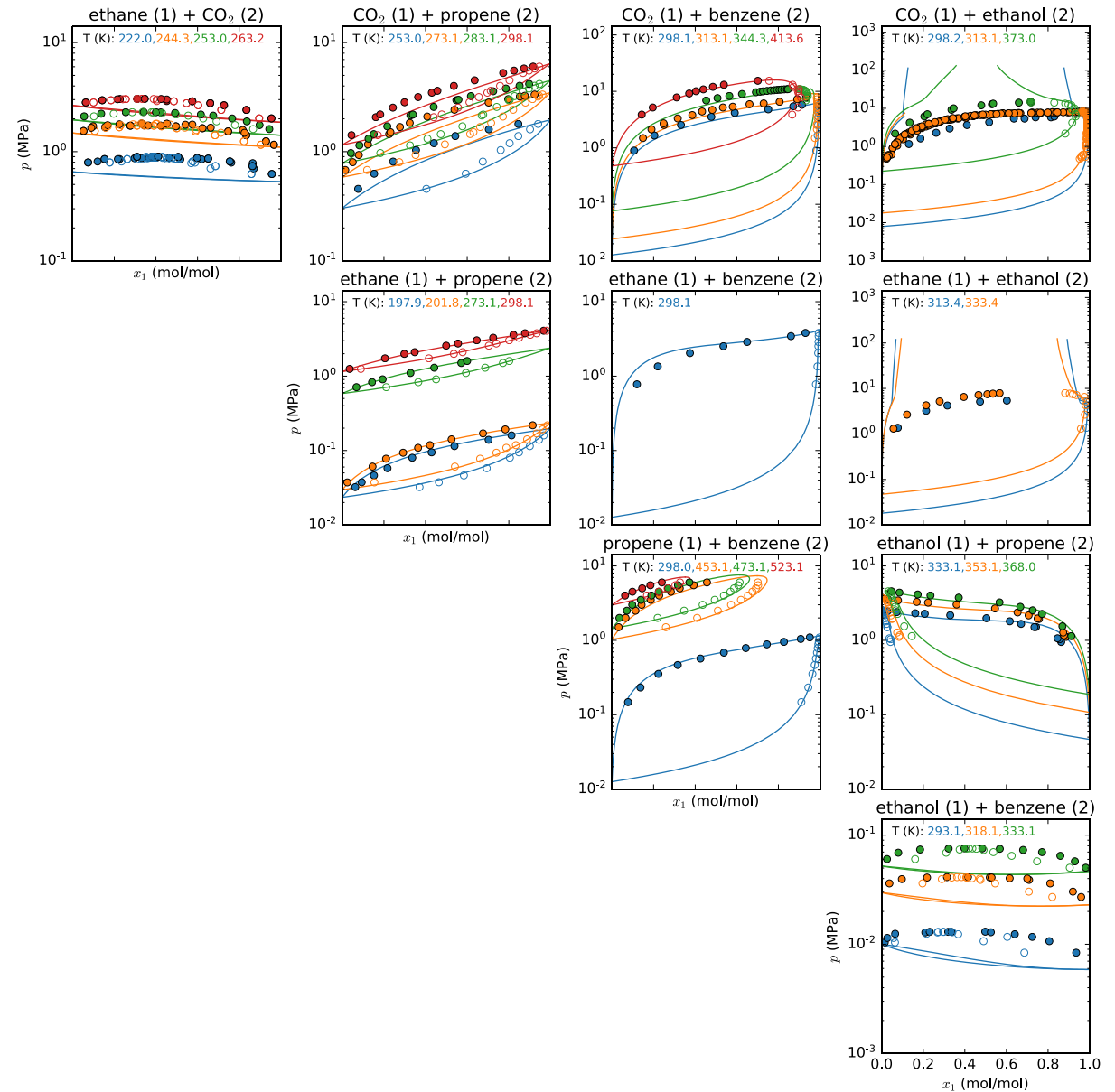


**For more results, see
 Jäger, A.; Bell, I.H.; Breikopf, C.: „A theoretically based departure function for
 multi-fluid mixture models“, Fluid Phase Equilibria 469, 56-69, 2018.**



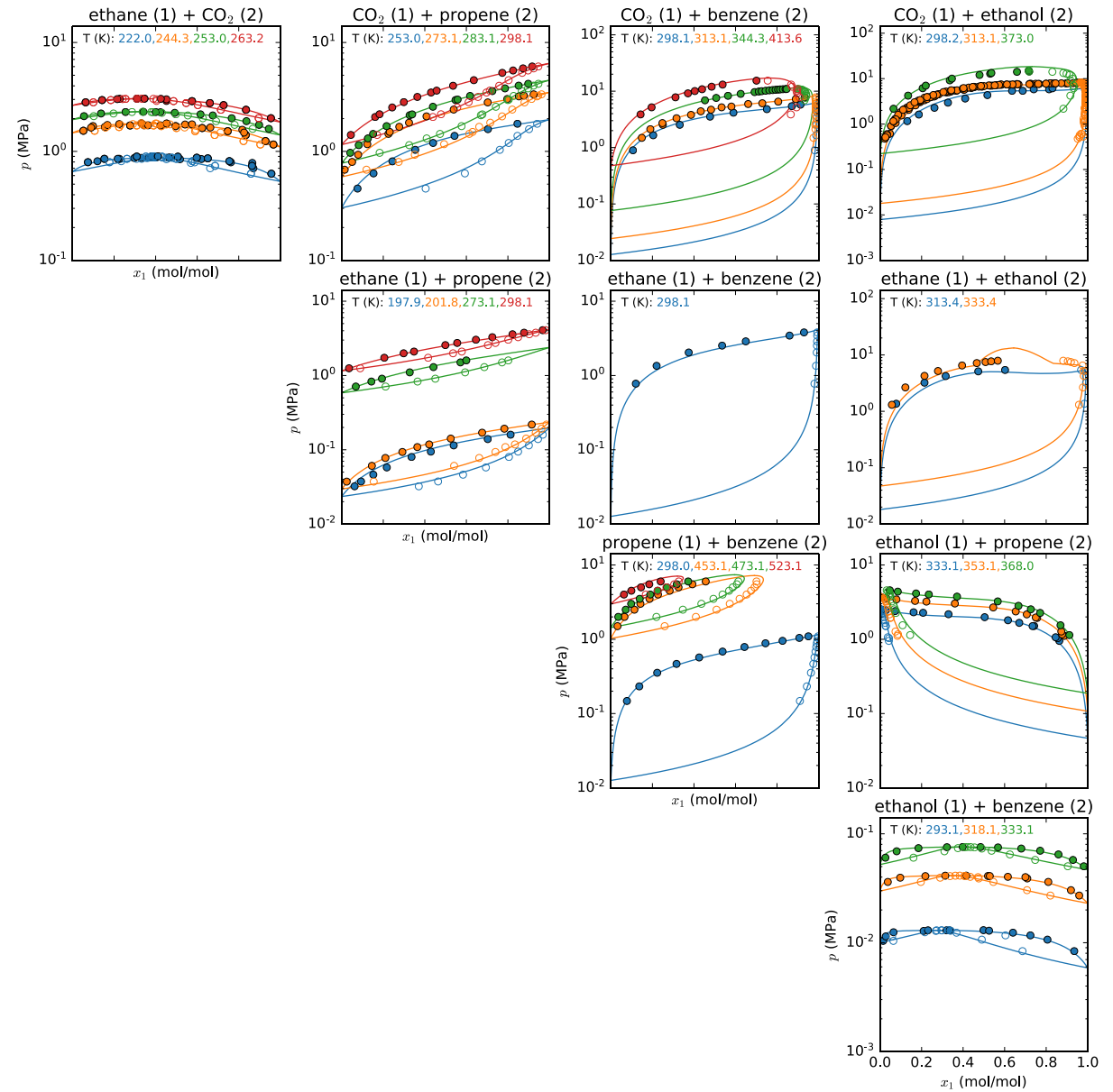
Results for all binary mixtures

— Linear mixing rules



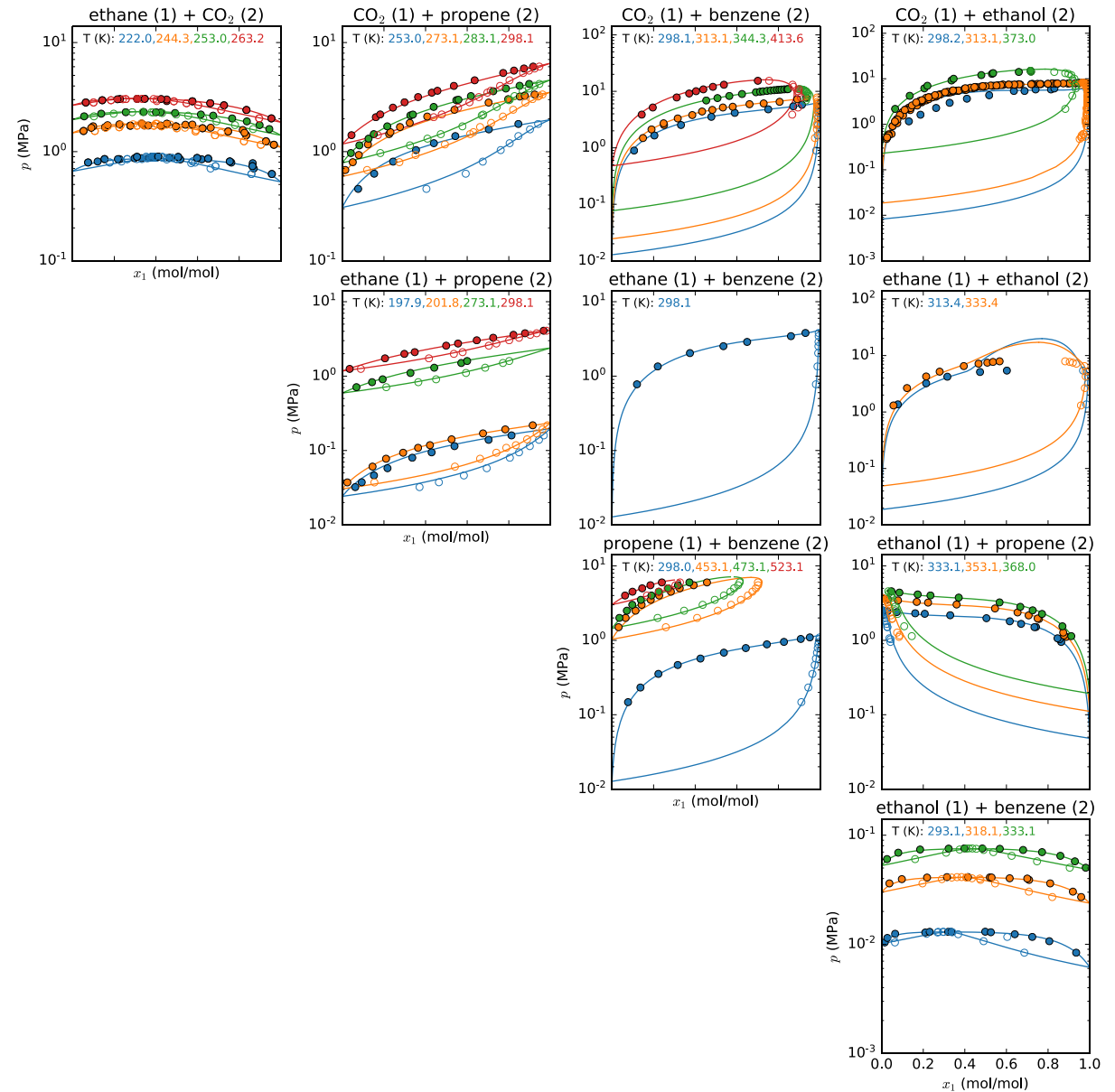
Results for all binary mixtures

— New model with fitted parameters



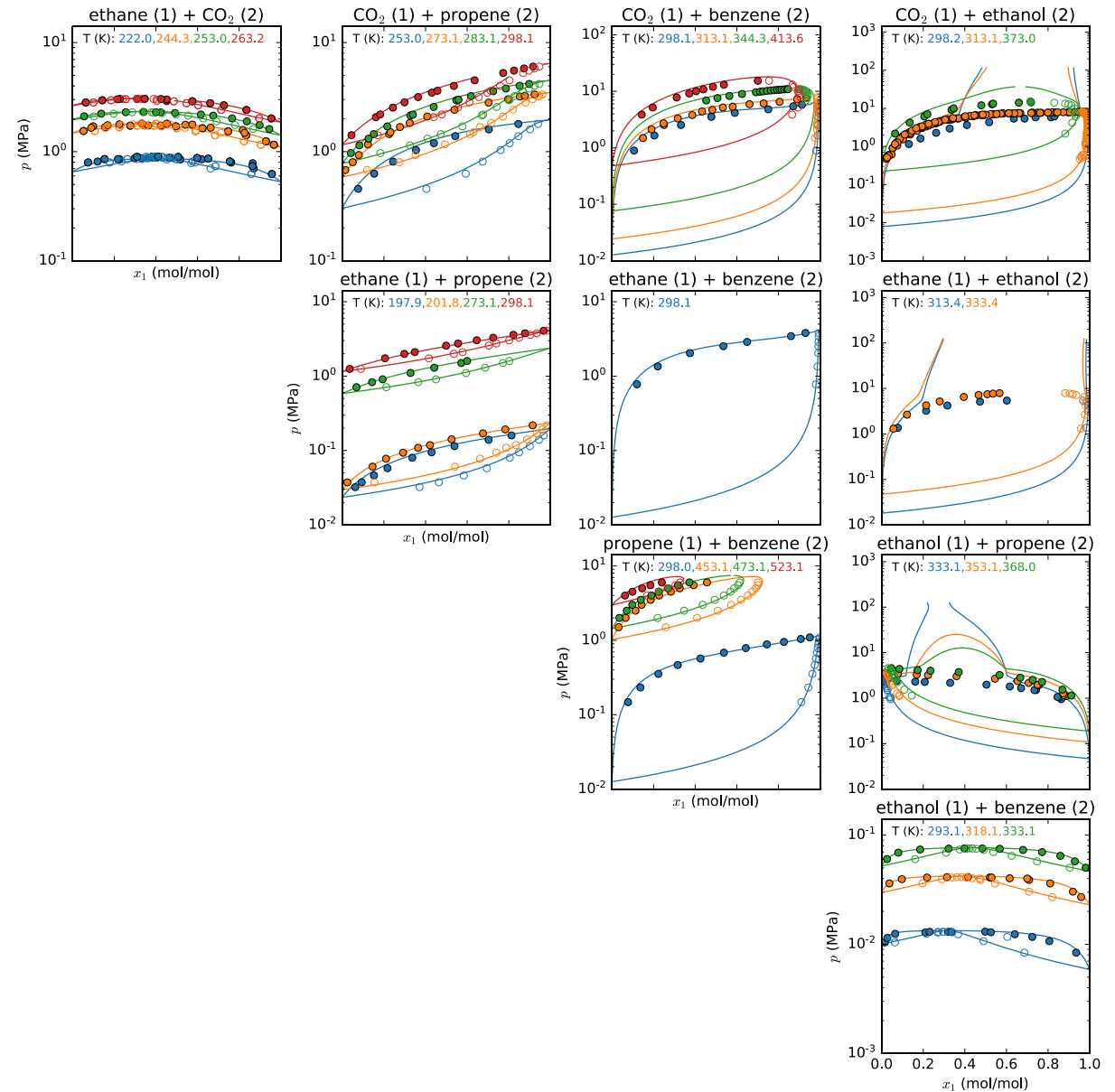
Results for all binary mixtures

— New model with PSRK parameters



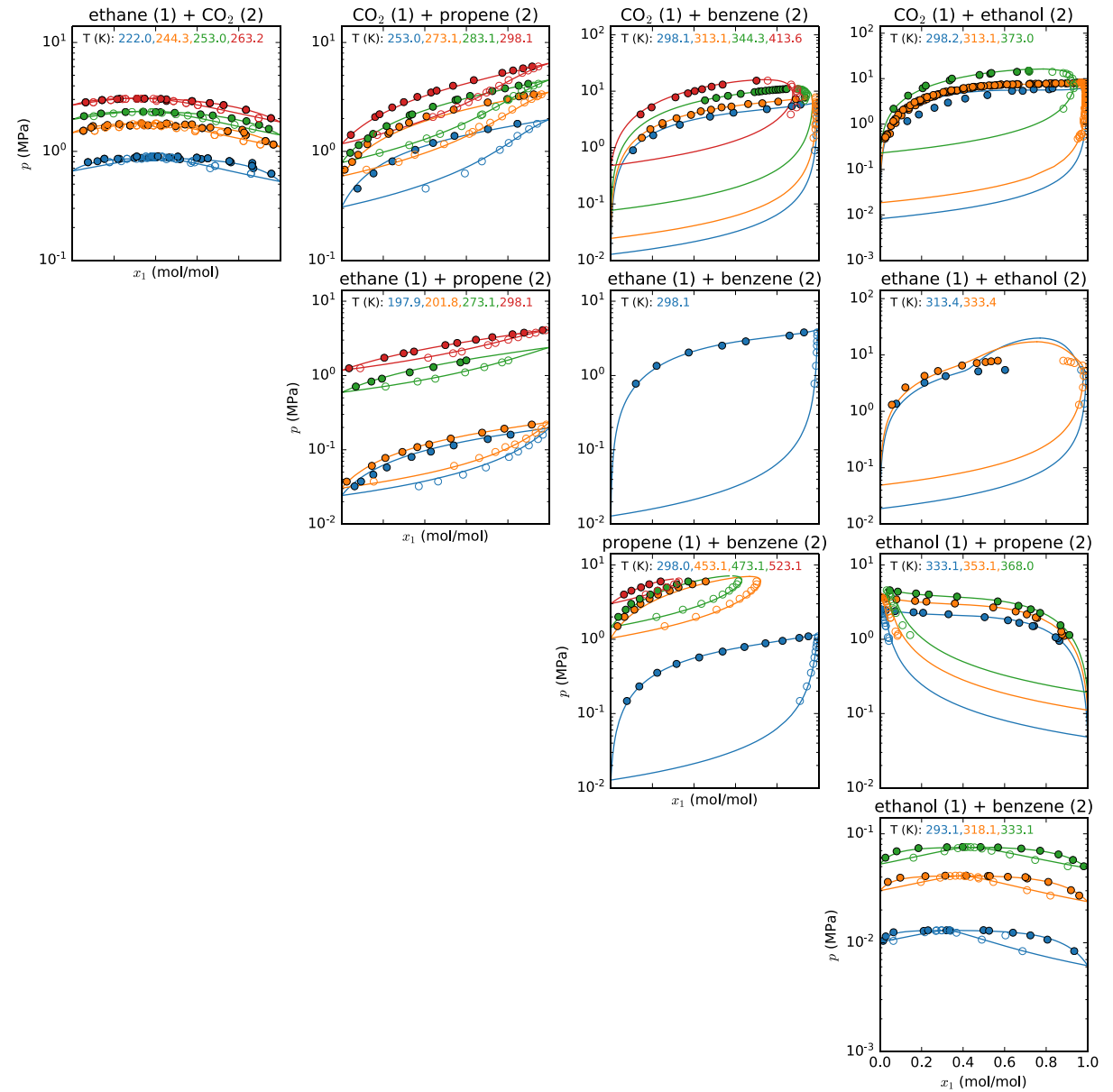
Results for all binary mixtures

— New model with VTPR parameters



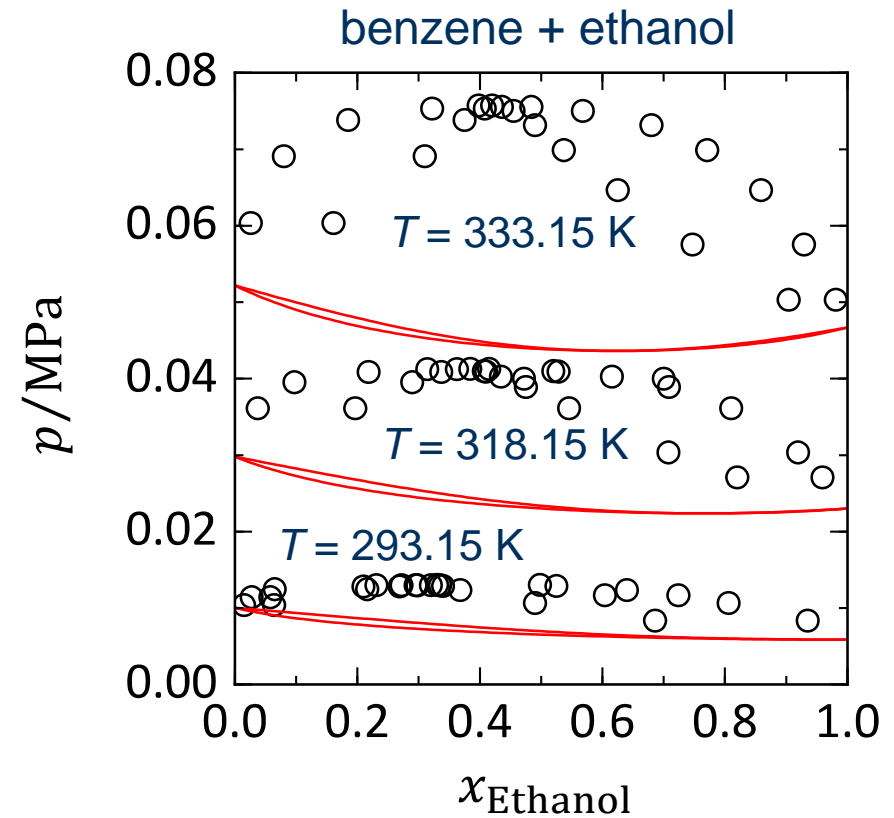
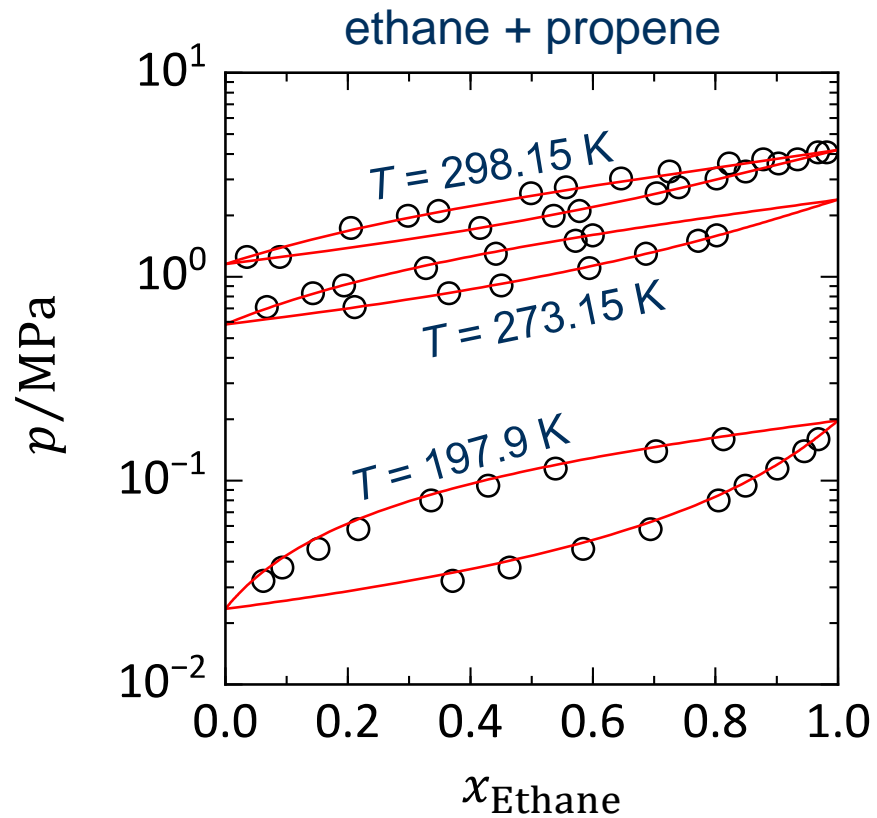
Results for all binary mixtures

— Results of full PSRK



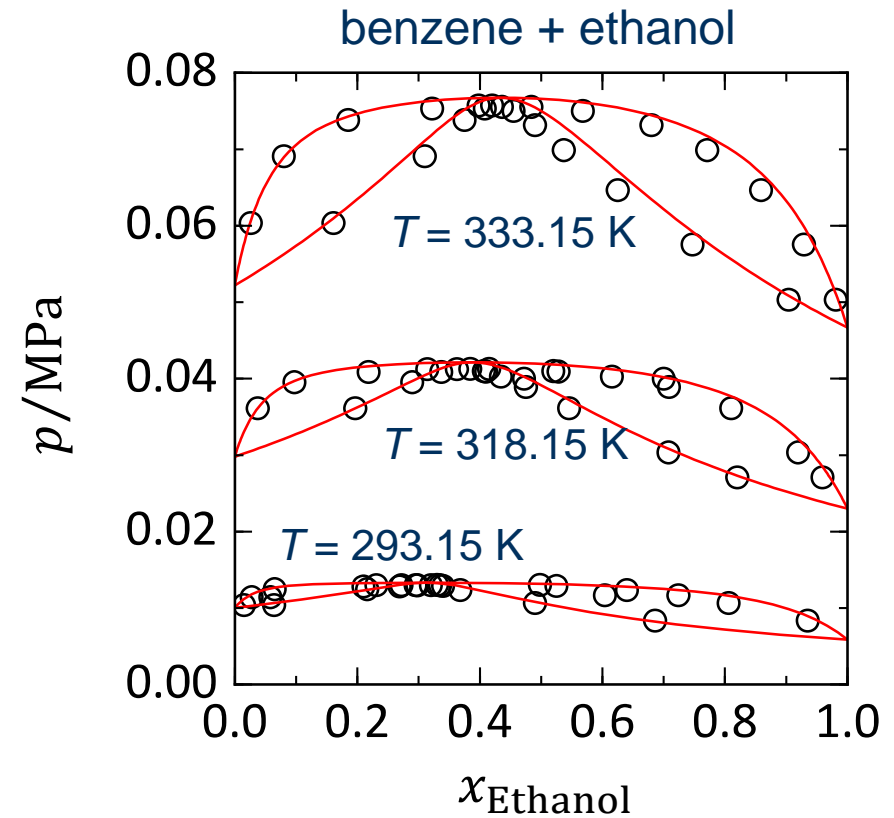
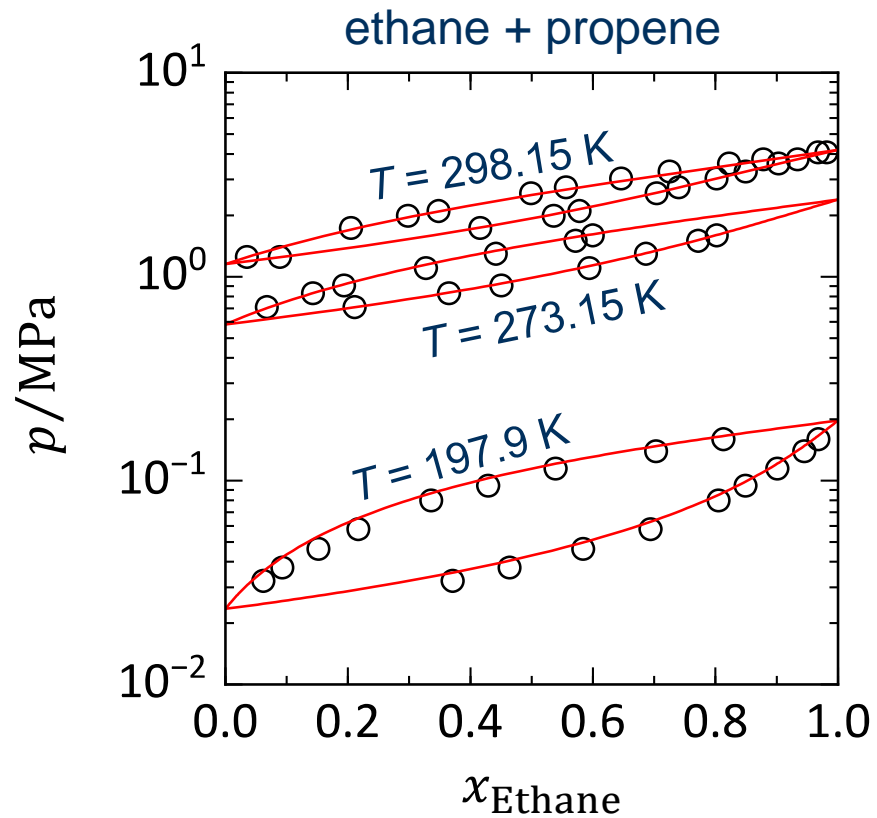
Results with Standard Mixing Rules

Results for ethane + propene and benzene + ethanol with **linear mixing rules**



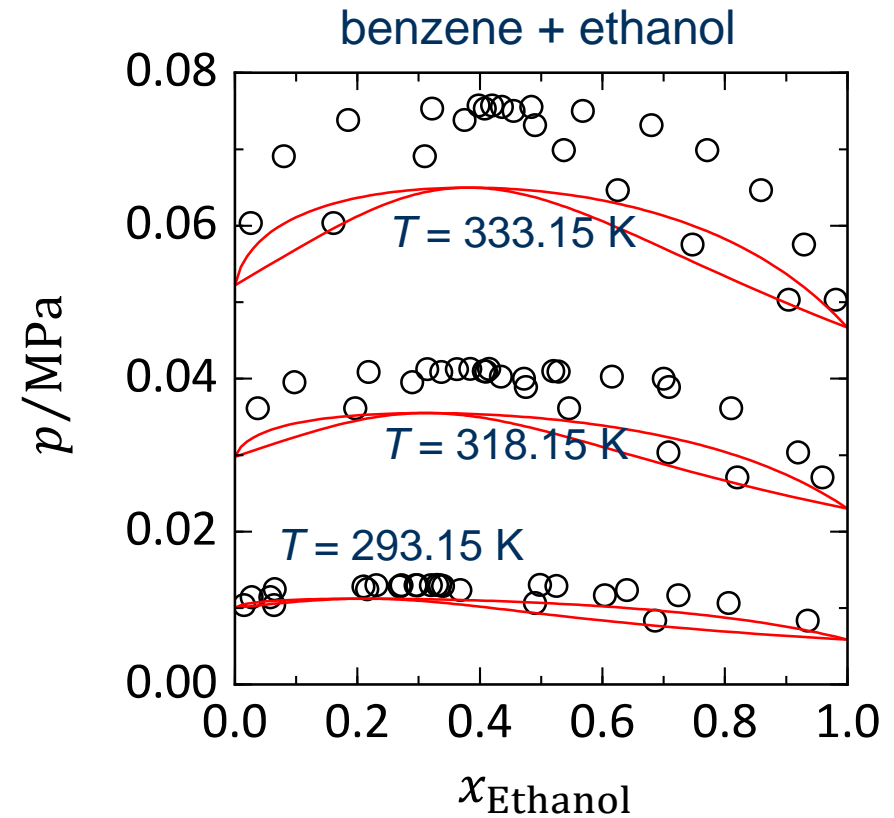
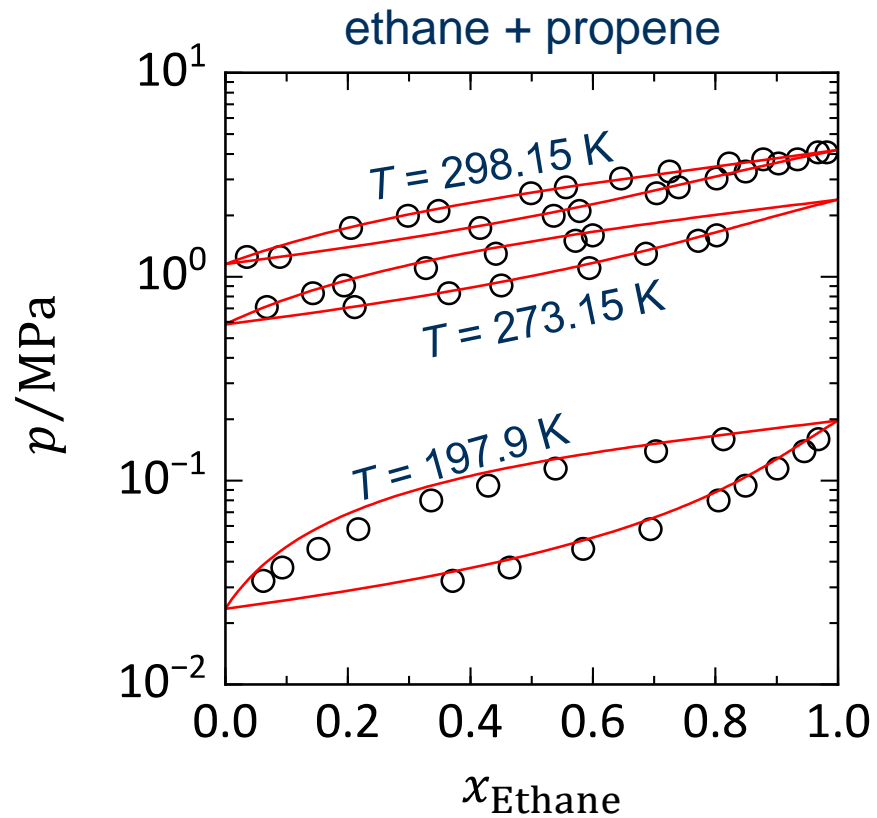
Results of the New Model with UNIFAC (VTPR) Parameters

Results for ethane + propene and benzene + ethanol with VTPR parameters for UNIFAC



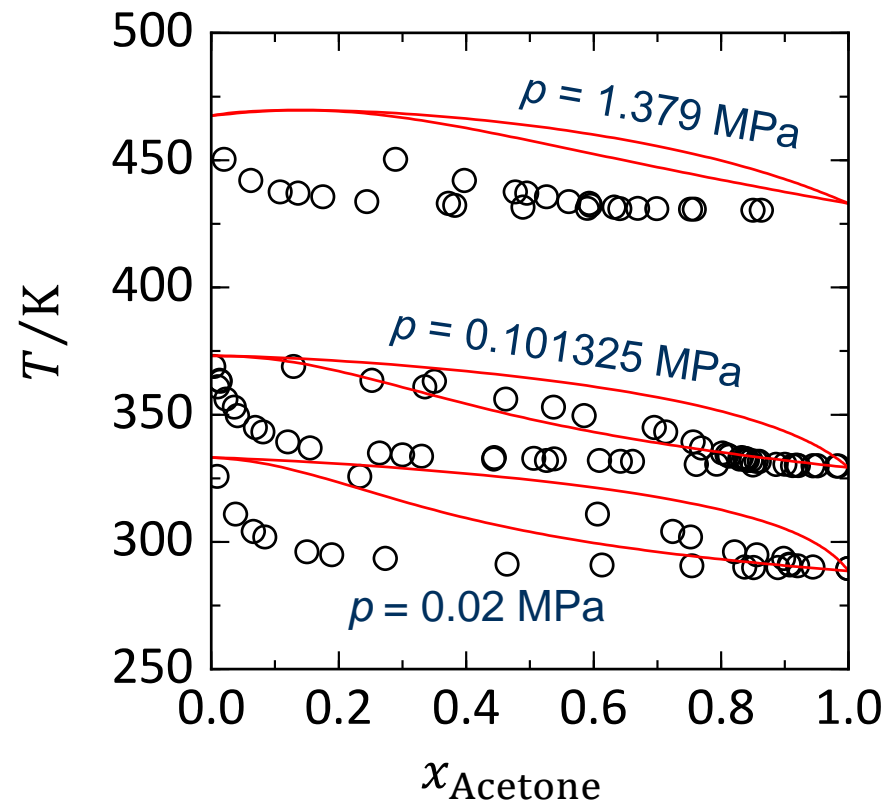
Results of the new model with COSMO-SAC (Mullins et al. 2006)

Results for ethane + propene und benzene + ethanol with COSMO-SAC



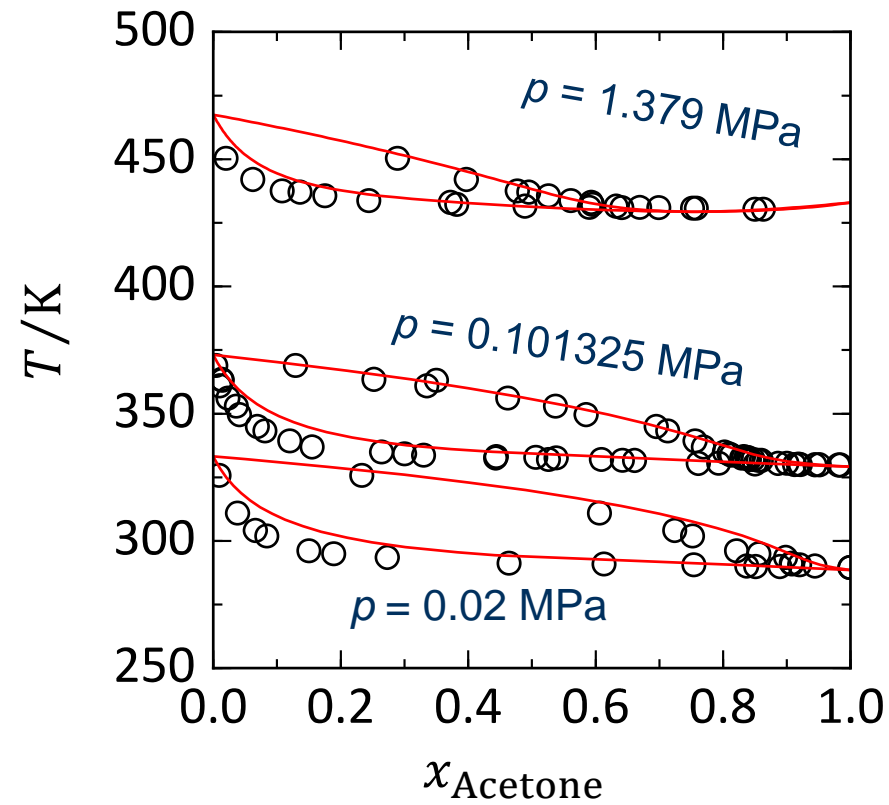
Results for mixtures with water: water + acetone

Results for acetone + water with **linear mixing rules**



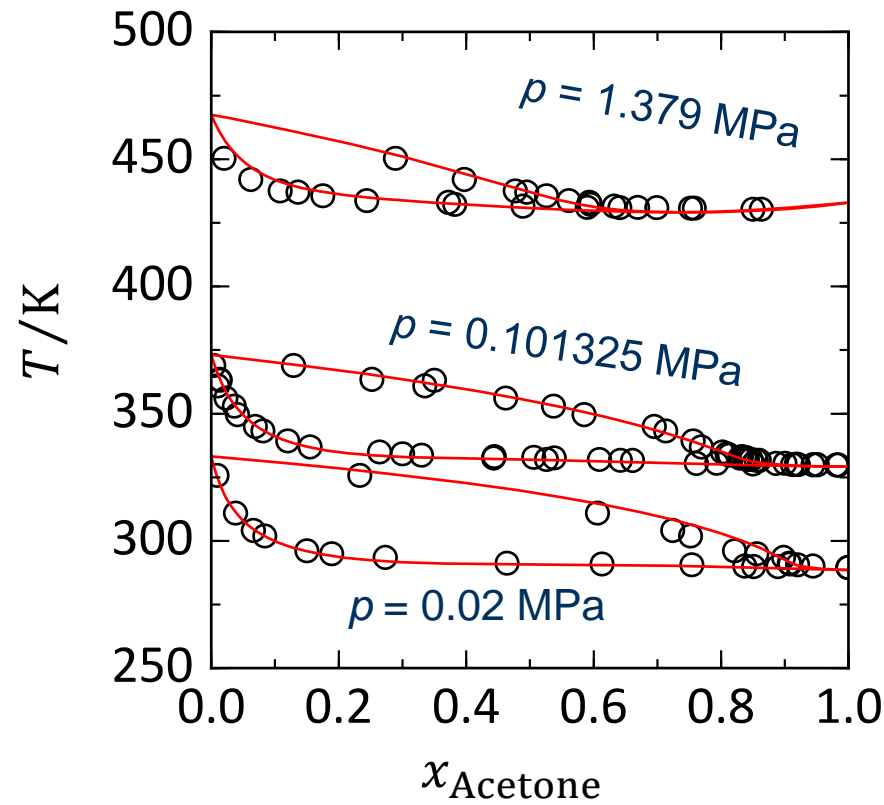
Results for mixtures with water: water + acetone

Results for acetone + water with **VTPR** parameters for **UNIFAC**



Results for mixtures with water: water + acetone

Results for acetone + water with partly fitted VTPR parameters for UNIFAC



Fitted to data:

$a_{79}, b_{79}, c_{79}, a_{97}, b_{97}, c_{97}$